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# Effect of preparation method on Indium-based materials, and their activity for CO<sub>2</sub> hydrogenation to methanol

Experimental degree thesis

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# **Abstract**

Methanol synthesis through CO<sub>2</sub> hydrogenation reaction seems to be a promising approach to mitigate the excess of CO<sub>2</sub> anthropogenic emissions in the atmosphere and substitute the traditional syngas-based CH<sub>3</sub>OH synthesis process. In<sub>2</sub>O<sub>3</sub> has recently attracted growing interest as a highly selective and stable catalyst for this reaction, and zirconia has been reported as a potential support to significantly improve In<sub>2</sub>O<sub>3</sub> catalytic activity. In this work, the effect of the preparation methods on the material and catalytic properties of both pure In<sub>2</sub>O<sub>3</sub> and mixed In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> were investigated. Three main methods were employed, namely the solution combustion, urea hydrolysis, and coprecipitation using three different precipitating agents (ammonia solution, sodium carbonate, and sodium oxalate). Additionally, the role of Pd was also studied with a series of In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub>-Pd samples prepared by the urea hydrolysis method. Various characterization techniques were used to characterize the physicochemical properties of the catalysts, including X-Ray diffraction (XRD), Scanning Electron Microscopy (SEM) Energy-Dispersive X-ray (EDX), N<sub>2</sub> physisorption, CO chemisorption, H<sub>2</sub>-TPR, O<sub>2</sub>-TPD, CO<sub>2</sub>-TPD, and X-ray Photoelectron Spectroscopy (XPS). The catalytic tests were performed in a flow-plug reactor at 40 bar.

The preparation method and the composition strongly influenced the physicochemical properties of the materials and their catalytic performances. In general, the  $ZrO_2$  introduction significantly improved the performance of the pure  $In_2O_3$ . Pd played a role as a promoter although the effect was not significantly pronounced in the tested samples due to a substantially narrow range of the Pd loadings. Indeed, among the  $In_2O_3$ - $ZrO_2$ -Pd samples, the max yield of methanol at 300 °C was obtained with the sample IZP-0.50, having a medium loading among the three tested catalysts. The absolute max yield of methanol production was achieved with the catalyst prepared with the coprecipitation using sodium carbonate at 300 °C which was comparable with those reported in the literature: this catalyst had a STY of 107.54 mmol  $g_{In}^{-1}$   $h^{-1}$ .

# Keywords

 $In_2O_3$ 

CO<sub>2</sub> hydrogenation

Methanol synthesis

Preparation method

 $ZrO_2$ 

Palladium

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# 1. Introduction

It is now taken for granted that the emission of greenhouse gasses (GHGs), such as CO<sub>2</sub>, CH<sub>4</sub>, and many other molecules, are driving the average global temperature to unprecedented temperatures that will cause serious harm to nature's equilibria and therefore humankind. Regrettably, CO<sub>2</sub>-emitting technologies have been a true nerve center of the economic and social growth of the human population, and they are now the backbone of the present-day society, together with other resources-depleting activities (e.g., fossil fuel extraction, mining, ...). The concern about GHGs emissions has recently increased the public, institutional and scientific consideration on more sustainable technologies, especially in energy production and in renewable energies (REs): the energy collected from renewable resources that are naturally replenished, such as sunlight, wind, rain, tides, waves and geothermal heat.



Figure 1 United Nations Sustainable Development Goals (SDGs).<sup>1</sup>

An important step forward in the institutional role in the climate change topic was made in December 2015, at the Conference of Parties in Paris (COP21), where delegates from 195 countries agreed to "pursue efforts to limit the (global average) temperature increase to 1.5 °C above pre-industrial levels, recognizing that this would significantly reduce the risks and impacts of climate change". This agreement went down in history as the "Paris Agreement", and was signed after the publication, in September 2015, of the United Nations Sustainable Development Goals, known as SDGs (Figure 1), for a social, economic, and climatic sustainable future. In order to reach a carbon zero-emission future, a transition to renewable

and non-fossil-based energy sources is essential. During the COP21 a second scenario, called "2-degree scenario" (or 2DS), was discussed to be the "point of no return", beyond which climate change will most probably be strongly destabilizing and unreversible. In this perspective, the average world temperature cannot increase to 2 °C above the pre-industrial levels.<sup>2</sup>

Sadly, the complete turn point of this transition now appears to be further than the prefixed by the 2DS and current data is showing us that humankind is on the edge of the cliff for a climate disaster. Anthropogenic emissions need to peak within 5 years from now to maintain realistically the COP21 targets; and primary sources consumption needs to drop to a quarter the current use, before 2100.<sup>3</sup>

#### 1.1 Scenarios

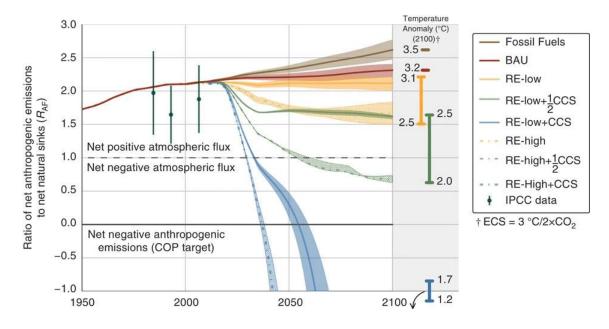


Figure 2 Ratios are calculated annually as the ratio between anthropogenic net C emissions, to net C sequestration by global plant, soil, and ocean systems. The shaded areas represent the scenarios sensitivity. Global surface temperature anomalies projections (DT) in 2,100 are indicated at the right, where each colored bar treats the RE-Low and RE-High scenarios as the endpoints of a continuous range of energy sector decarbonization.<sup>3</sup>

By examining Figure 2, taken by the work of Walsh, *et al.*,<sup>3</sup> with a business-as-usual (BAU) scenario, therefore by keeping the same current growth trends in decarbonization, we would reach a peak after 2050, missing target maximum temperature increase of 1.5 °C. The term "decarbonization" stands for an abatement in the carbon net emission by a multitude of anthropogenic activities. Even the REs scenarios, where REs grow is virtually boosted at 5.0%

annually, in line with aggressive climate action, will not be enough to respect the target. Full decarbonization relies on the coupling of CCS (Carbon Capture and Sequestration, or CCSU that stands for Carbon Capture, Sequestration, and Utilization, or CSS<sup>4</sup> that stands for Carbon Sequestration and Storage) technologies, bioenergy production, and REs implementation. With a full industry transition, humans will need to couple the capture of the anthropogenic CO<sub>2</sub> excess to avoid going beyond the point of no return.

# 1.2 Carbon Capture, Storage and Utilization (CCSU)

Anthropogenic carbon dioxide capture and storage is much different from the natural processes behind natural carbon sinks: it has been estimated that approximately 50% of anthropogenic CO<sub>2</sub> emissions are reabsorbed by the oceans and terrestrial land sinks, taking, respectively, 25% each.<sup>5</sup> This seems to play a role of assistance, but these natural carbon sinks act like an ecological buffer, via chemical and ecological feedbacks, which is slowly going to deteriorate the more CO<sub>2</sub> we are going to emit. Furthermore, this carbon dioxide adsorbed by ecological sinks remains an extra amount, out of balance, that causes problems, as soil and ocean acidification, and therefore we are going to need to answer for this distress anyway.<sup>6</sup>

# 1.2.1 Carbon Capture

Two are the methods for carbon capture: Direct Air Capture (DAC), from the atmosphere, and point-source capture, from the flue gasses of one-point sources of emission, such as industrial plants, power generators, and vehicles. On paper, the DAC is the most tempting, since the capture station can be installed anywhere, its dimensions do not need to respect any plant and no existing plant would need the implementation to adapt to the carbon capture; but the low concentration of CO<sub>2</sub> in the atmosphere (slightly above 400 ppm) is a huge thermodynamic obstacle.<sup>7</sup>

On the other hand, the point source capture would be more feasible and efficient, since the CO<sub>2</sub> concentration in the stripped outlet stream of a plant lays between 3 and 35%; the CO<sub>2</sub> capturing process can be performed by post-combustion, pre-combustion, or oxyfuel capture methods.<sup>8</sup> This system, however, is appliable only to large source points, like industrial plants and power generators, and not too small (but numerous) point sources as vehicles; furthermore, transport

and storage infrastructures would need to be close to the point source where CO<sub>2</sub> is captured if the utilization plant is not closeby.<sup>7</sup>

The research field of carbon capture has gained attention in the scientific community in recent years, nevertheless, several issues need to be solved, such as low efficiency in CO<sub>2</sub> capturing, lack of legislation, processes costs, and real environmental sustainability of the processes.

# 1.2.2 Storage versus Utilisation

Two are the possibilities of CO<sub>2</sub> employment of the post-capture application: direct carbon storage (CCS) or carbon utilization (CCU). The CCS option is coarser, but it has a high-volume potential over the overall human emissions, while the CCU is a more elegant solution (from the circular carbon economy point of view: "avoiding" emissions by reusing spent CO<sub>2</sub>) but a smaller impact by the percentage on the volumetric emissions. It is most likely that we are going to need a combination of the two techniques in the soon future, the so-called CCSU, to actualize the scenarios, even if chemical production from CO<sub>2</sub> will probably have a relatively minor role to play in terms of volume for CO<sub>2</sub> emission reduction. Having said that, its weight cannot be discounted because of the potential economic benefits and the increasing demand for the several carbon-based chemicals derived from fossil fuel sources (thus termed petrochemicals) that can be produced from CO<sub>2</sub>; furthermore, the storage facilities for CO<sub>2</sub> are limited.

# 1.3 Chemical valorization

The CCU intrinsically includes the concept of chemical valorization: the CO<sub>2</sub> is introduced back in the industry from a worthless and harmful scrap molecule to a more complex form of value-added products, such as biofuels, that have become a huge priority, or base chemicals, like methanol.<sup>8</sup> Carbon dioxide has also long been identified as one potential vector molecule to inject REs and their surplus peaks, into the energy chain, like other possible energy vectors (H<sub>2</sub>, ammonia, ...), while contributing to close the carbon cycle connected to CO<sub>2</sub> emissions and produce chemicals that can be easily inserted in the chemical production chain.<sup>4</sup> REs can be used or stocked directly in these processes (as solar thermal energy or geothermal heat), but most commonly it is converted into a secondary energy medium, as electricity, which is widespread and easy to introduce in the electricity grids.

Engaging now the chemical valorization route, a distinction must be drawn between base and fine chemicals: base chemicals are large volume products and thus with a higher effective fossil fuel consumption, that is potentially easier and larger to replace with REs direct inputs; fine chemicals, on the other hand, generally do not incorporate RE, except by an intermediate formation of chemicals, such as methanol, and their production is rather limited in terms of volume of products, and will thus have a minor impact in terms of CO<sub>2</sub> and REs consumption.<sup>10</sup>

Hereafter is shown a schematic overview (Figure 3) of the possible CO<sub>2</sub> conversion products, mostly base chemicals, their routes, and the potential ways to incorporate REs in these processes: methanol is the most interesting product, as a widely used raw material in the chemical industry and a possible intermediate to produce olefins.

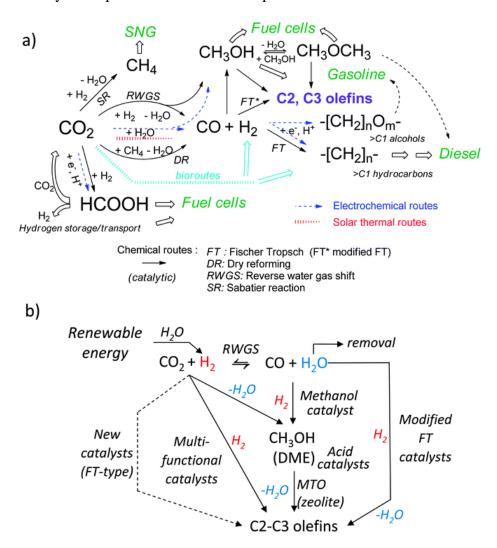


Figure 3 (a) Schematic overview of  $CO_2$  conversion routes and potential REs integration. The RE is either direct (solar thermal) or indirect (renewable  $H_2$  production, electrochemical routes). (b) Different possible routes to synthesize light olefines from  $CO_2$  and  $H_2$ .<sup>10</sup>

#### 1.3.1 Hydrogen's role

It is clear that H<sub>2</sub> is a key molecule for this class of reactions, and we are now widely aware that a carbon-free society will not be possible without a renewable H<sub>2</sub> economy: as it is outlined in Figure 3, H<sub>2</sub> is an energy and electron carrier, a fundamental base chemical and a key connector of REs and the chemical industry, in particular for the CO<sub>2</sub> valorization processes discussed previously; therefore, it is necessary to develop better and more efficient processes to produce H<sub>2</sub> from REs.<sup>11,12</sup> It is indeed true that most of the CO<sub>2</sub> reductions need hydrogenation, and for a sustainable application of CCU, hydrogen needs to be cheap and renewable. Currently, cheap H<sub>2</sub> comes from carbon-intensive fossil fuels-based processes (i.e., steam reforming of methane). A noncarbon-intensive approach for H<sub>2</sub> production is water electrolysis, which, however, is 3–4 times more expensive than H<sub>2</sub> produced from fossil sources,<sup>7</sup> and the sustainability problem is moved down the production chain from the raw materials to the energy used during the electrolysis. H<sub>2</sub> would need to be produced economically via water electrolysis using clean and/or renewable energy (e.g., wind, solar, nuclear, ...) to pursue the entire process sustainability.

# 1.3.2 Thermodynamics

Sadly, the stark reality of CO<sub>2</sub> needs to be addressed: its inertness and thermodynamic stability; carbon dioxide is the most stable end-product when dealing with carbon oxidation and the bigger is the thermodynamic "hurdle" we need to face, the harder the obstacle will be to cross. C-O bonds are stronger than C-H bonds, consequently, oxygenated products have higher stability compared with their hydrogenated counterparts (Figure 4). Furthermore, most of the products that can be obtained from CO<sub>2</sub> are liquid at atmospheric conditions, therefore the reactions are entropically unfavorable. The chemical transformation of CO<sub>2</sub> is thermodynamically more favorable when it is used as a co-reactant a molecule that has a higher Gibbs free energy such as H<sub>2</sub>. Based on these energetic premises, we can deal with two different CO<sub>2</sub> conversion categories: when the more energetic secondary reactant supply enough energy to the reaction to be exothermic and work without a catalyst (carboxylates and lactones, carbamates, urea, isocyanates, and carbonates); and when the reaction is not enough energetically favorable and it needs a considerable source of external energy plus a catalyst to overcome the high activation energy of the C=O breaking.<sup>7</sup>

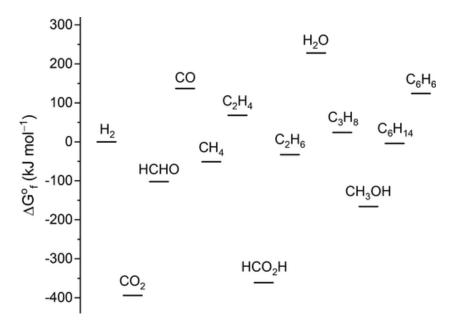


Figure 4 Gibbs free energy of formation ( $\Delta G_{0,f}$ ) for simple carbon compounds at different oxidation states of carbon;  $H_2$  and  $H_2O$  are included for their key role. Reprinted with permission from American Chemical Society.<sup>7</sup>

#### 1.3.3 Current status of chemical valorization

The inertness and thermochemical stability of CO<sub>2</sub> lead the research to prioritize the study of new active, selective, and stable catalysts; multiple catalytic pathways are now a matter of investigation by research groups.

A young and alternative strategy for CO<sub>2</sub> transformation is photocatalysis, but the efficiency is substantially lower than the targeted amount for CO<sub>2</sub>-involving reactions;<sup>13</sup> the research is mainly focused on thermal or electrochemical catalytic reduction.<sup>14</sup> So far, the electrochemical reduction has the huge advantage to extract the needed H<sub>2</sub> from the water molecule in the medium, allowing the avoidance of the use of gas H<sub>2</sub>, but technical problems are still huge, as the small scale required and the difficulties in the scale-up process.<sup>15</sup> The traditional thermochemical processes are right now the most promising, thanks to the abundant pre-existing literature on other akin processes and the presence of industrial plants that can easily be adapted to CO<sub>2</sub> hydrogenation. Homogeneous catalysts are now out of the picture for many reasons (hard separation, poor process economy, and small processable volumes) and this leads to the research on heterogeneous catalysts.<sup>16–18</sup>

# 1.4 Methanol

Methanol (CH<sub>3</sub>OH or MeOH) is the simplest alcohol in its family, liquid at ambient conditions, and a flammable, toxic and harmful chemical. It is one of the main C<sub>1</sub> (molecules containing one C atom) platform chemicals and together with ethylene, propylene, benzene, toluene, and xylenes, it is among the most demanded petrochemicals worldwide.<sup>19</sup> With an annual growth rate of 6 % between 2014 and 2019,<sup>20</sup> methanol had a production capacity of 157.27 million metric tons in 2020 and it is forecasted to double within 2030.<sup>21</sup>

Other than being a chemical commodity for the synthesis industry, it is also a fuel additive and a potential sustainable fuel itself. To tackle the problem of energy storage and, in parallel, the discontinuity and surplus peaks in renewable energies, methanol could be employed as an energy carrier molecule of the Power-to-X (PtX) processes that stock energy, such as the electricity peaks in renewables, in another storable form, as chemical energy; this compound can then be fed to another process (e.g., combustion, fuel cells, ...). The PtX process can lead to liquid energy carriers (PtL), as in the case of methanol, or gaseous energy carriers (PtG), as in the case of methane, another potential candidate. Operational costs analysis suggests that methanol synthesis has the highest overall efficiency compared with methane since CH<sub>3</sub>OH does not require compression and decompression, has a higher volumetric energy density, and lower transportation costs.<sup>22</sup>

# 1.4.1 Methanol synthesis history

In 1913 the German company BASF synthetized methanol from syngas (Reaction (1), a mixture of CO and  $H_2$ ) obtained from coal, by using a zinc/chromium oxide catalyst;<sup>23</sup> 10 years later the same company built the first commercial methanol synthesis plant operating at very high temperature and pressure (300 - 400 °C, 250 - 350 atm).

(1) CO + 2H<sub>2</sub> 
$$\rightleftharpoons$$
 CH<sub>3</sub>OH,  $\Delta$ H° = -90.5 kJ mol<sup>-1</sup>

Years after, at the beginning of the 1960s Cu was discovered to be active toward the production of methanol from natural gas and naphtha<sup>24</sup> and the Imperial Chemical Industries achieved a new industrial process operating at milder conditions (200 - 300 °C, 50-100 atm). Since then, Cu-based materials have always been employed in industrial methanol production through syngas.<sup>23</sup>

The commercial heterogeneous catalyst Cu-ZnO-Al<sub>2</sub>O<sub>3</sub> usually contains 50 - 70 atomic % CuO, 20 - 50 % ZnO and 5 - 20% of the Al<sub>2</sub>O<sub>3</sub> promoter. The industrial catalyst is also able to convert to methanol a small percentage of CO<sub>2</sub> present in the gas inlet feed of the industrial process, bearing the water produced by RWGS reaction without its activity being affected. Considering the activity towards CO<sub>2</sub> and the present literature behind it, Cu-ZnO-Al<sub>2</sub>O<sub>3</sub> was the first and most studied catalyst for CO<sub>2</sub> hydrogenation to methanol.<sup>25</sup>

#### 1.4.2 Reaction conditions and thermodynamics

During the process of CO<sub>2</sub> hydrogenation to methanol, two reversible reactions are involved: CH<sub>3</sub>OH is produced via CO<sub>2</sub> hydrogenation (Reaction (2)) while CO is generated via reverse water-gas shift reaction (RWGS, Reaction (3)):

(2) 
$$CO_2 + 3H_2 \rightleftharpoons CH_3OH + H_2O$$
,  $\Delta H^{\circ} = -49.4 \text{ kJ mol}^{-1}$ 

(3) 
$$CO_2 + H_2 \rightleftharpoons CO + H_2O$$
,  $\Delta H^{\circ} = +41.2 \text{ kJ mol}^{-1}$ 

The CO formed in the RWGS reaction may also react itself with  $H_2$  to produce more methanol (Reaction (4)):

(4) CO + 
$$2H_2 \rightleftharpoons CH_3OH$$
,  $\Delta H^{\circ} = -90.5 \text{ kJ mol}^{-1}$ 

During the process we aim at the Reaction (2) and (4), exothermic and with an increase in the moles of the product: according to Le Châtelier's principle, the favorable conditions are high pressure and low temperature. While the parasitic RWGS is endothermic and occurs without changes in the total number of molecules, therefore it is favored by high temperatures, while pressure has no thermodynamic effect on the reaction equilibrium. The industrial methanol synthesis employs a pressure of 50-100 bar, <sup>26</sup> but, although the thermodynamics lead to low temperatures reaction, the kinetic limits the hydrogenation and therefore force to use high temperatures to increase the methanol formation kinetics. As in every commercial process involving low conversion rates toward the products, the unreacted stream is cycled back into the reactor to increase the overall efficiency. Concerning the feed ratio, the H<sub>2</sub>/CO<sub>2</sub> volumetric ratio employed is usually 3/1, but the increase of the ratio leads to a higher conversion of CO<sub>2</sub> to methanol due to the sensitivity of this reaction to hydrogen partial pressure.<sup>27</sup>

# 1.5 Catalysts for CO<sub>2</sub> hydrogenation to methanol

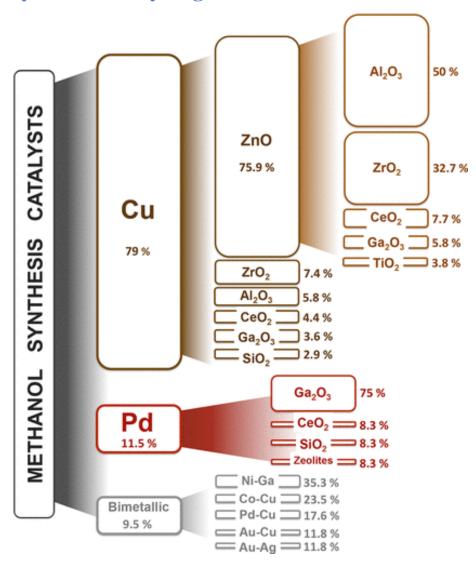


Figure 5 Types of catalyst material reported for  $CO_2$  hydrogenation to methanol in ca. 200 paper published between 2006 and 2016. The marked percentages represent the amount of literature for each material in the whole revised literature. Reprinted with permission from Elsevier.<sup>23</sup>

Figure 5 displays the catalytic materials reported in almost 200 publications over 10 years, from 2006 to 2016 and it is taken from a review of Álvarez A., *et al.*, submitted the 07.12.2016.<sup>23</sup> The relative areas and percentages show how frequently those materials have been reported in the studied collection, and it emerges that the most relevant class of catalysts has been the Cu-based family, in particular the Cu-ZnO-Al<sub>2</sub>O<sub>3</sub>. This latter material, bearing in mind the activity towards CO<sub>2</sub> and the present literature behind it, was the first and therefore the most studied catalyst for CO<sub>2</sub> hydrogenation to methanol.<sup>25</sup>

# 1.5.1 Traditional Cu-ZnO-Al<sub>2</sub>O<sub>3</sub> catalyst

As for CO hydrogenation to methanol, in the CO<sub>2</sub> counterpart Cu acts as the active species, ZnO is a promoter and a matrix that allows achieving a high dispersion of Cu, whereas the alumina (Al<sub>2</sub>O<sub>3</sub>) enhances the thermochemical stability of the solid. The ZnO role as a promoter is taken for granted, but its specific mechanism is still under debate: one possibility could be the important role of the Cu-ZnO interface in the CO<sub>2</sub> activation, while the second possibility is the role of a ZnCu bimetallic alloy formed by partial reduction during the reaction. The reaction over Cu is proven to be quite structure-sensitive, therefore the preparation method is a key point. Typically, the preparation is carried out with the simple and effective coprecipitation method (Figure 6), through which it is easy to reach a high dispersion and the high stability of the Cu species.<sup>7</sup>

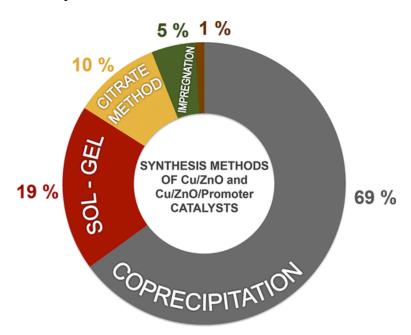


Figure 6 Synthesis methods of Cu–ZnO and Cu–ZnO–promoter catalysts. The marked percentages were calculated based on ca. 200 publications published between 2006 and 2016. Reprinted with permission of Elsevier.<sup>23</sup>

Although the catalyst has a low price and it is remarkably active towards the hydrogenation reaction, it also suffers from a rapid deactivation due to the water formation as one of the main by-products of the parasitic reaction of Reverse Water Gas Shift (RWGS),<sup>28</sup> that also reduces the selectivity of the catalyst towards CH<sub>3</sub>OH. This is moreover the limiting factor behind the shallow percentage of CO<sub>2</sub> in the feed stream supported in the syngas-based process. One drawback of this catalyst is that it shows poor activity at low temperature (< 250 °C) and the presence of H<sub>2</sub>O induces a strong temperature- and water-induced deactivation of Cu particles by carbon deposition, and Cu oxidation and sintering.<sup>29</sup> These limitations undermined the value

of the catalyst for the reaction of hydrogenation, pushing the research to find new catalyst families or to stabilize the Cu-ZnO-Al<sub>2</sub>O<sub>3</sub> from deactivation, for instance, the employment of membrane reactors that remove water during the reaction.<sup>16,30</sup>

# 1.5.2 New non-Cu-based catalysts

In recent years, some different catalytic systems were found to be more active and performant than the Cu-ZnO- $Al_2O_3$  system. These new catalyst families deal with the activity and stability issues of the traditional catalyst.

#### 1.5.2.1 Intermetallic materials and oxides

Research has revealed that some intermetallic systems are more active than the conventional Cu-ZnO-Al<sub>2</sub>O<sub>3</sub> catalyst towards the CO<sub>2</sub> hydrogenation to methanol, thanks to a reduced RWGS activity that hindered the methanol selectivity, different reaction kinetics, and higher stability of the standard catalyst. For instance, Ni-Ga catalysts (particularly Ni<sub>5</sub>Ga<sub>3</sub>) on silica showed high selectivity and suppression of the RWGS reaction.<sup>31</sup> A bimetallic In@Co system showed a superior performance thanks to an abundance in O-vacancies promoted by the Co support;<sup>32</sup> PdZn supported on CeO<sub>2</sub> had an excellent H<sub>2</sub>-dissociation ability of the bimetallic alloy,<sup>33</sup> as well as Pd-Cu bimetallic catalyst, that showed a better mechanism of adsorption and dissociation of both CO<sub>2</sub> and H<sub>2</sub>.<sup>34</sup> Intermetallic systems are also a cost-effective alternative unless noble metals are a substantial part of the chemical composition.

Metal oxides such as CeO<sub>2</sub>, Ga<sub>2</sub>O<sub>3</sub>, ZrO<sub>2</sub>, and TiO<sub>2</sub> exhibit a fair catalytic activity and methanol selectivity, while the activity of certain oxides, such as ZnO and most importantly In<sub>2</sub>O<sub>3</sub>, stands out;<sup>35</sup> this is going to be investigated later on in this thesis.

#### 1.5.2.2 Pd-based catalysts

Like in many catalytic reactions, noble metals, such as Pd, are attractive and have already been employed (Figure 5) due to their attractive characteristic: stability, resistance to sintering and poisoning, strong tendency to form allows, and activity towards H<sub>2</sub> adsorption, splitting and spillover.<sup>35–37</sup> Pd has the remarkable capability of easily adsorbing the H<sub>2</sub> in H<sub>2</sub>\* (\* represents a surface-adsorbed species) and split the molecule into two active H\* (H<sub>2</sub>-splitting); After this dissociative chemisorption happened the adsorbed atomic hydrogen is capable of migrating

along the Pd surface and spill over the support material (hydrogen spillover). The support can then be reducible, as TiO<sub>2</sub>, ZrO<sub>2</sub>, or ZnO, or non-reducible, as SiO<sub>2</sub> or Al<sub>2</sub>O<sub>3</sub>.<sup>38</sup> These features allow Pd to move atomic hydrogen from sites to the reactive species and complete the catalytic cycle. Having said that, these catalysts suffer, however, from low selectivity, stringent high cost, and weak CO<sub>2</sub> binding.<sup>39</sup>

# 1.5.3 Role of the support

As well as metal-metal interactions, metal-support interactions can boost the stability and activity of a catalyst. For instance, Yang, *et al.*,<sup>40</sup> observed a stabilizing effect of Ce oxide on a system of Au NPs deposited over a CeO<sub>x</sub>/TiO<sub>2</sub> support, thanks to CeO<sub>x</sub>'s electronic polarizing nature. As is going to be addressed later in this thesis (1.6.1 Active sites), oxygen vacant sites are important active sites in the activity of oxides and other active phases on CO<sub>2</sub> hydrogenation reaction. A support that drives the formation of oxygen vacancies is beneficial for CO<sub>2</sub> adsorption, stabilization of reaction intermediates, and lifespan of the catalyst. For example, a CeO<sub>2</sub> support showed this beneficial promotion of oxygen vacancies on a bimetallic PdZn alloy<sup>33</sup>, just as a Co oxide,<sup>32</sup> or a monoclinic ZrO<sub>2</sub>,<sup>41</sup> incremented the number of O vacant sites on In<sub>2</sub>O<sub>3</sub> active phase supported on these oxides.

# 1.6 In<sub>2</sub>O<sub>3</sub>

Before its application in CO<sub>2</sub> hydrogenation, In<sub>2</sub>O<sub>3</sub> was studied in the Methanol Steam Reforming (MSR) reaction, until a DFT calculation, published in 2013, suggested the potential of its catalytic application in methanol synthesis from CO<sub>2</sub>.<sup>35</sup> The first methodical article that inquired into the likely active bulk In<sub>2</sub>O<sub>3</sub> was the work of Martin O., *et al.*,<sup>42</sup> published in 2016, where the research group addressed already the promoting abilities of ZrO<sub>2</sub> support, and the key role of the oxygen vacancies in the catalyst activity and stability.

 $In_2O_3$  exhibits higher methanol selectivity than Cu, Co, and noble metal catalysts and higher catalytic activity than other oxides, such as ZnO. It can also be easily supported and modified, giving accessibility to tailoring for reactants activation sites or stabilization of the intermediates. For instance, the support can influence the presence and abundance of Ovacancies on the surface of  $In_2O_3$ , largely accepted as critical role players in the catalyst activity.

#### 1.6.1 Active sites

During the hydrogenation reaction,  $In_2O_3$  can be easily reduced to  $In_2O_{3-\delta}$  generating a large number of oxygen vacancies ( $O_v$ ) on its surface. Most of the studies on the catalytic activity of In oxide indicate that the missing O atom creates an ideal active site for the adsorption of one O atom from the  $CO_2$  molecule and its consequent activation.<sup>35</sup> Furthermore  $O_v$  can stabilize key reaction intermediates and reduce the over-reduction of  $In_2O_3$  to In metallic and its consequent deactivation.<sup>47</sup> A possible catalytic cycle involving  $O_v$  can be visualized in Figure 7: the two oxygen atoms are adsorbed in the  $O_v$  in the  $In_2O_3$  surface lattice by the positively charged In atoms allowing a consecutive addition of protons obtained by the heterolytic splitting of  $H_2$ . During the reaction, methanol formation replenishes the oxygen vacancy sites, whereas  $H_2$  helps to regenerate the vacancies. But not only  $O_v$  are active towards  $CO_2$  hydrogenation: other types of active sites are reported as activation sites for the  $CO_2$  molecule, such as metallic and acid-base sites.<sup>48</sup>

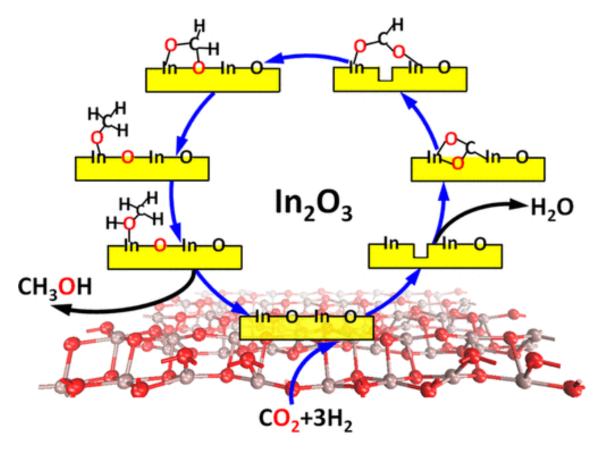


Figure 7 Active oxygen vacancy site for CO<sub>2</sub> hydrogenation to methanol on the defective In<sub>2</sub>O<sub>3</sub>(110) surface and one of its possible catalytic cycles. Reprinted with permission from Elsevier.<sup>49</sup>

Furthermore, In<sub>2</sub>O<sub>3</sub> exhibits higher catalytic activity and methanol selectivity than other metal oxides, such as CeO<sub>2</sub>, Ga<sub>2</sub>O<sub>3</sub>, ZnO, ZrO<sub>2</sub>, and TiO<sub>2</sub>.<sup>50–52</sup> The correlation of these oxides activity towards the reaction and their CO<sub>2</sub> adsorption energy is clear: the weaker the interaction between the oxides surface and CO<sub>2</sub>, the poorer their catalytic activity; but in case this adsorption energy is too strong, like with ZnO,<sup>53</sup> could hinder the correct activation of the CO<sub>2</sub> molecule (Table 1).

Table 1 Calculated CO<sub>2</sub> and CO Adsorption Energies, E<sub>ad-CO<sub>2</sub></sub> and E<sub>ad-CO<sub>3</sub></sub>, on the Metal Oxide Surfaces.<sup>35</sup>

	Ead-CO2 (eV)	Ead-CO (eV)
In <sub>2</sub> O <sub>3</sub>	-0.61	-0.89
ZnO	-1.26	-1.40
Ga <sub>2</sub> O <sub>3</sub>	-0.31	-0.81
CeO <sub>2</sub>	-0.19	-0.28
ZrO <sub>2</sub>	-0.24	-0.37
TiO <sub>2</sub>	-0.17	-0.34

The methanol formation competes with the parasitic RWGS reaction, and the CO adsorption energies (Table 1) are directly related to the product distribution. A lower  $E_{ad-CO}$  indicates that the generated CO can be desorbed more easily, resulting in a high CO selectivity.<sup>35</sup>

#### 1.6.2 Reaction mechanism

Understanding the mechanism of the reaction is fundamental for the reaction optimization: by knowing all the reaction paths, its intermediates, the active sites, and active species, research can tailor the materials to boost the reaction activity through, for instance, stabilization of the key reaction intermediates or enhancement of active sites properties.

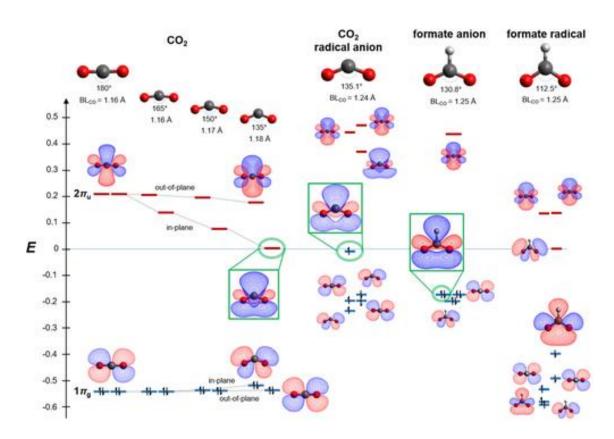


Figure 8 Orbital energy diagrams with characteristic OCO angle and CO bond length, for linear and bent forms of CO<sub>2</sub>, radical CO<sup>2-</sup>, formate ion, and formate radical. The energy scale is in Hartree.<sup>54</sup>

The activation of CO<sub>2</sub> starts from the linear equilibrium geometry of O=C=O: the molecule needs to be bent to break its symmetry and its chemical inertness (Figure 8). By inducing changes in its shape, we can modify the energy level of its molecular orbitals, elongating and weakening the C=O bonds; this makes the C atom more heterophilic and more prone to be attacked to form an active radical anion of CO<sub>2</sub>.<sup>54</sup> On the other hand, hydrogen is dissociated on the In<sub>2</sub>O<sub>3</sub> surface by heterolytic route, resulting in one negatively charged H (hydride) bound to In and one positively charged H (proton) bound to O.<sup>35</sup>

Experimental and theoretical studies have been carried out to understand the reaction's mechanism.  $^{49,55-57}$  As shown in Figure 9 two possible reaction pathways are likely to happen, namely, the formate (HCOO\*) path and the carboxyl (COOH\*) path; in the first, CO<sub>2</sub> is hydrogenated by In–H to form a formate species, while in the second, CO<sub>2</sub> is protonated by O–H to form a bicarbonate species. A third less likely path, responsible for the parasitic RWGS reaction, may be possible, namely RWGS + CO-hydro pathway. Most studies have confirmed that the formate pathway (CO<sub>2</sub>  $\rightarrow$  HCOO\*  $\rightarrow$  H<sub>2</sub>CO\*  $\rightarrow$  H<sub>3</sub>CO\*  $\rightarrow$  CH<sub>3</sub>OH) on oxygen vacancies of the In<sub>2</sub>O<sub>3</sub> surface is the most favorable route, although the COOH\* route and

RWGS + CO-hydro route may both be possible. However, the fundamental understanding of the active sites and reaction mechanism is still under investigation and needs to be clarified. Moreover, questions concerning  $In_2O_3$  long-term stability with Time On Stream (TOS), the pathways of catalyst deactivation, and regeneration are still to be addressed.<sup>58</sup>

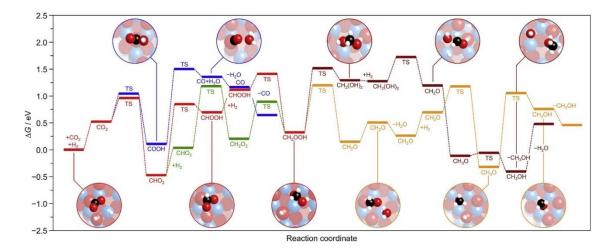


Figure 9 Gibbs energy profile for  $CO_2$  hydrogenation through the most representative paths. C is represented as black, O as red, H as white, In as light blue. The hydrogenation of  $CO_2$  to  $CH_2OOH$  is shown in red; from this species, the two possible routes to  $CH_3OH$  are depicted in orange and brown. The alternative formation of  $CH_2OOH$  from  $CHO_2$  through the co-adsorption of two  $H_2$  molecules is shown in green. RWGS reaction is marked in blue. Conditions: P = 5 MPa and T = 573 K. TS = transition state. Reprinted with permission from Elsevier.  $^{56}$ 

# **1.6.3 Support**

As for the vast majority of heterogeneous catalysts, a support is indicated for various reasons: a general boost in the activity, cost reduction, increment in properties as surface area, porosity, catalyst stability, and therefore, minor deactivation. To boost In<sub>2</sub>O<sub>3</sub> features, multiple carriers with distinct nature were explored. The optimal was achieved through the tuning of chemical, physical, and geometric properties of both ZrO<sub>2</sub> and In<sub>2</sub>O<sub>3</sub>,<sup>41,59</sup> that induced a remarkable improvement of the intrinsic activity of the unsupported oxide, with almost a 10-fold higher STY per gram of indium.<sup>42</sup>

#### 1.6.3.1 ZrO<sub>2</sub>

Gao, *et al.*,<sup>52,60</sup> synthesized by coprecipitation an indium–zirconium composite oxide with a higher specific surface area than the sole In<sub>2</sub>O<sub>3</sub> and a reaction rate of approximately five times the one of bulk In<sub>2</sub>O<sub>3</sub>. When In<sub>2</sub>O<sub>3</sub> is deposited on a ZrO<sub>2</sub> support, its activity and stability during CO<sub>2</sub> hydrogenation to methanol are increased.<sup>42,55</sup> DFT calculations showed that a ZrO<sub>2</sub>

support can inhibit the dissociation of CO<sub>2</sub> into CO on In<sub>2</sub>O<sub>3</sub>, reducing the relevance of the RWGS kinetic pathway, stabilizing key intermediates of the formate pathway, <sup>44</sup> and enhancing the adsorption of CO<sub>2</sub>. <sup>61</sup>

In addition to increasing the dispersion of the active phase, ZrO<sub>2</sub> also facilitates the formation of oxygen vacancies, and these can stabilize the key reaction intermediates and facilitate the adsorption and activation of the reactants on the In oxide surface. 42,44,52,60

In the case of deposited In<sub>2</sub>O<sub>3</sub> on ZrO<sub>2</sub>, one possible O<sub>v</sub> formation trigger could be the presence of Zr<sup>3+</sup> species in ZrO<sub>2</sub> before the active phase deposition, which could abstract oxygen atoms from the active phase upon calcination or reaction. <sup>41,42,62</sup> Phase, morphology, and preparation method of the catalyst are key decisions on the catalytic potential of the material. A remarkable case is a study carried out by Frei, *et al.*, <sup>41</sup> where they observed a considerably higher activity for an active phase deposited on a monoclinic-ZrO<sub>2</sub> compared to a more common tetragonal-ZrO<sub>2</sub> support. Phase, morphology, and preparation methods will be displayed in the following chapters.

The india loading on the zirconia support has, obviously, a fundamental impact on the final material performances. In one distinctive article, Yuan C, *et al.*,<sup>55</sup> showed that by varying the indium loading between the narrow 0.1 -5 wt % range, the selectivity to both methanol and CO can reach 80 % in the broad temperature range 250 – 280 °C. It is proposed a synergic effect between highly dispersed india and the ZrO<sub>2</sub> substrate, which allows to highly tune the crystallinity of In<sub>2</sub>O<sub>3</sub>, the dimensions of the particles, and the reaction pathways that the reactants can take. Crystalline In<sub>2</sub>O<sub>3</sub> in intimate contact with ZrO<sub>2</sub>, prevails for loadings over 2.5 wt.%, while highly dispersed In<sub>2</sub>O<sub>3</sub> dominates for loadings below 0.5 wt.%. At loadings of 2.5 – 5 wt.% the material bonds modestly with the formate pathway intermediates (\*HCOO and \*H<sub>3</sub>CO), resulting in an optimized selectivity toward methanol. However, at lower indium loadings than 2.5 wt.%, strong bonding of \*HCOO impedes methanol synthesis.

# 1.6.4 H<sub>2</sub>-splitting promoter

In the hydrogenation of CO<sub>2</sub> to CH<sub>3</sub>OH, the H<sub>2</sub>dissociation step plays a crucial role in the reaction rate; however, the activity towards H<sub>2</sub> is limited for the sole In<sub>2</sub>O<sub>3</sub> phase. Doping In<sub>2</sub>O<sub>3</sub> with noble metals is a possible strategy to enhance the dissociation of H<sub>2</sub> and the H-spillover onto the In<sub>2</sub>O<sub>3</sub> surface, hence increasing the reaction rate. Moreover, Pd-based catalysts have

been already widely studied for the synthesis of  $CH_3OH$  from CO at low temperatures<sup>63,64</sup> and  $CO_2$ ,<sup>45,65–67</sup> as is shown in Figure 5. Pd shows to be among the best choices, but other noble metals alternatives such as  $Au^{68}$ ,  $Ir^{69}$ , Pt70, and  $Rh^{71}$  have been studied.

The activation of hydrogen does not just play a role during the reaction, but it is also conducive to the formation of oxygen vacancies in the catalyst activation. The H-spillover from the noble metal to the In oxide can promote the formation of oxygen vacancies on the  $In_2O_3$  by reduction of  $In^{3+}$  and snatching away O atoms by  $H_2O$  formation.<sup>45</sup>

The Pd species that is truly active during the hydrogenation of CO<sub>2</sub> to methanol is controversial: there is no evidence that the phase of Pd on the surface of In<sub>2</sub>O<sub>3</sub> remains under reaction conditions because most of the characterization techniques are employable before the reaction and after it, *ex-situ*. It is, however, proven as true that InPd intermetallic compounds have a good ability to activate H<sub>2</sub> and they play a role in the hydrogenation reaction, with even 70 % higher rates as compared with the traditional Cu-ZnO-Al<sub>2</sub>O<sub>3</sub> catalyst.<sup>72–74</sup> Despite the good activity it is important to notice that the formation of an InPd intermetallic phase means a significant amount of Pd and a major economic burden.

Another drawback of Pd employment is its activity for the parasitic RWGS reaction, in particular in the presence of a SiO<sub>2</sub> support:<sup>74</sup> high-nuclearity Pd clusters thermodynamically advantage the formation of CO over CH<sub>3</sub>OH, therefore maintaining small particle sizes is fundamental.<sup>35</sup> Furthermore, bigger Pd particles retain more H<sub>2</sub>O, thus facilitating In<sub>2</sub>O<sub>3</sub> deactivation by sintering. To overcome this issue, Perez-Ramirez, *et al.*,<sup>66</sup> recently adopted a coprecipitation method to incorporate isolated Pd atoms in the In<sub>2</sub>O<sub>3</sub> lattice. By doing so, Pd was embedded into indium oxide pockets, avoiding its clustering during the synthesis. When the solid was then calcined and exploited in the reaction the Pd atoms formed low-nuclearity Pd clusters on the In oxide surface. The apparent activation energy of the RWGS reaction was increased by -7 kJ mol<sup>-1</sup> compared with a case with a catalyst with the same Pd loading prepared via dry impregnation method.

# 1.6.5 Phase and morphology

The phase and morphology of all the counterparts that participate during the reaction are central in the catalytic study of a material. With phase and morphology greatly vary properties of the heterogeneous catalyst, both micro-characteristics, such as the crystalline pattern, facets exposed to the reaction and types of  $O_v$ , and macro characteristics, like the total exposed surface area of the material and its porosity.

There are three crystal structures reported in the literature for In<sub>2</sub>O<sub>3</sub>: the cubic bixbyite-type phase (c-In<sub>2</sub>O<sub>3</sub>), the hexagonal corundum-type phase (h-In<sub>2</sub>O<sub>3</sub>), and the orthorhombic Rh<sub>2</sub>O<sub>3</sub>type phase (o-In<sub>2</sub>O<sub>3</sub>). <sup>75,76</sup> The O<sub>v</sub> on the different crystal phases (c-In<sub>2</sub>O<sub>3</sub> and h-In<sub>2</sub>O<sub>3</sub>) exhibit different catalytic performances for CO<sub>2</sub> hydrogenation. For instance, Wang, et al., <sup>77</sup> found that it is easier to adsorb H<sub>2</sub> and to form oxygen vacancies on the surface of c-In<sub>2</sub>O<sub>3</sub>, and these oxygen vacancies adsorb CO<sub>2</sub> strongly, compared with h-In<sub>2</sub>O<sub>3</sub>. Dang, et al., <sup>78</sup> found the oxygen vacancies' properties varies with the crystal type and facet: h-In<sub>2</sub>O<sub>3</sub> (104) facet can stabilize greatly key intermediates involved in methanol formation and give higher methanol selectivity c-In<sub>2</sub>O<sub>3</sub>. Besides, their results show that CO<sub>2</sub> adsorption strength follows the order of h-In<sub>2</sub>O<sub>3</sub> (104) > c-In<sub>2</sub>O<sub>3</sub> (110) > c-In<sub>2</sub>O<sub>3</sub> (111)  $\approx$  h-In<sub>2</sub>O<sub>3</sub> (012). Shi et al., <sup>79</sup> synthetized c-In<sub>2</sub>O<sub>3</sub>, h-In<sub>2</sub>O<sub>3</sub>, and a mixed cubic/hexagonal- In<sub>2</sub>O<sub>3</sub> (c/h-In<sub>2</sub>O<sub>3</sub>) catalysts with a controllable hydrothermal/solvothermal method. They showed that c/h-In<sub>2</sub>O<sub>3</sub> has a significant mixedcrystal effect resulting from the phase mixing, which leads to better textural properties, more O<sub>v</sub>, higher CO<sub>2</sub> adsorption strength and capacity, and thus higher conversion of CO<sub>2</sub> and STY of CH<sub>3</sub>OH (about 2 times higher), compared to single-phase In<sub>2</sub>O<sub>3</sub> catalysts. Furthermore, after use, the mixed-phase oxide has no obvious change, being very stable and too difficult to reduce during the hydrogenation.

The phase of the ZrO<sub>2</sub> support drastically influences the extent of In<sub>2</sub>O<sub>3</sub> reduction, its structural evolution during the hydrogenation, and, therefore, its activity. Notably, monoclinic ZrO<sub>2</sub> (m-ZrO<sub>2</sub>) showed pronounced effects on deposited In<sub>2</sub>O<sub>3</sub> due to the lattice mismatching and consequent tensile stress in the In<sub>2</sub>O<sub>3</sub> lattice.<sup>41</sup> The phenomenon was not present on In<sub>2</sub>O<sub>3</sub>/t-ZrO<sub>2</sub> (tetragonal ZrO<sub>2</sub>) which had a 1 order of magnitude lower STY. The tensile forces stabilized In<sup>2+</sup>/In<sup>3+</sup> sites in the In<sub>2</sub>O<sub>3</sub>, which create active In-O<sub>v</sub>-In and In- O<sub>v</sub>-Zr surface species, a key parameter in the high stability and activity of the In<sub>2</sub>O<sub>3</sub>/m-ZrO<sub>2</sub> catalyst.<sup>47</sup> Both t-ZrO<sub>2</sub> and m-ZrO<sub>2</sub> have enabled an epitaxial alignment, or epitaxy (a well-define crystalline deposition of a material over another crystalline seed), of the In<sub>2</sub>O<sub>3</sub> on their surface, but only

m-ZrO<sub>2</sub> has applied this unsettling tensile force.<sup>41</sup> Furthermore, CO<sub>2</sub> is activated to a greater extent on m-ZrO<sub>2</sub> than on t-ZrO<sub>2</sub>, as was already proved for the similar Cu/ZrO<sub>2</sub> catalysts.<sup>80,81</sup>

Tsoukalou, *et al.*,<sup>47</sup> reported that the phase of ZrO<sub>2</sub> significantly affects the local structure, reducibility, and catalytic performance of In<sub>2</sub>O<sub>3</sub> NPs deposited on a ZrO<sub>2</sub> support for the hydrogenation of CO<sub>2</sub> to methanol. For example, in contrast to m-ZrO<sub>2</sub>, the a-ZrO<sub>2</sub> support promotes the rapid reduction of In<sub>2</sub>O<sub>3</sub> to metallic In, leading to an almost inactive catalyst. The t-ZrO<sub>2</sub> support avoids the complete conversion to In<sup>0</sup>, but the extent of reduction is substantial, with an average oxidation state of In below +2, associated with poor catalytic activity.

Adopting coprecipitation methods for the material synthesis, even the formation of an india–zirconia solid solution phase may also play a significant role in catalyst activity. Employing this promising preparation method, the maximum interaction between the two metal oxides is reached, yet solid solutions of In<sub>2</sub>O<sub>3</sub> with t-ZrO<sub>2</sub> showed an inferior catalytic performance in comparison to supported In<sub>2</sub>O<sub>3</sub>/m-ZrO<sub>2</sub> and In<sub>2</sub>O<sub>3</sub>/t-ZrO<sub>2</sub> catalysts.<sup>41,82,83</sup>

As it was examined in the second half of the previous paragraph "1.6.4 H<sub>2</sub>-splitting promoter", the promoter's phase and morphology characteristics are crucial: either the presence of Pd<sup>0</sup> or intermetallic PdIn species, or the dimension and distribution of the particles can substantially vary the catalyst performances, such as RWGS pathway selection, or the H<sub>2</sub>-splitting and hydrogen spillover final characteristics.

# 1.6.6 Preparation method

As in all the branches of heterogeneous catalysis, the synthesis method of the material, its post-synthesis, and activation treatment are the groundwork on which the performance of the catalyst stands. The method employed, all its conditions, from the initial to the final, the timings, and the chemicals employed are a few of the countless parameters that can influence the final performance of the material: the active phase mode of introduction on its support varies their same interaction, and phase and morphology of the solid largely depends on the preparation method conditions.

One clear example is given by Frei, *et al.*,<sup>41</sup> that demonstrate that an  $In_2O_3$ – $ZrO_2$  material synthesized via coprecipitation formed a solid solution which resulted in an inferior activity, whereas the deposition synthesis formed sub-nanometric islands of  $In_2O_3$  under tensile stress, which triggered the formation of an excess of  $O_v$  and enhanced its activity. Again, Perez-

Ramirez, *et al.*, <sup>66</sup> adopted a coprecipitation method to incorporate Pd atoms in the In<sub>2</sub>O<sub>3</sub> lattice and showed that Pd was embedded into indium oxide pockets, avoiding its clustering during the synthesis, and when the solid was then calcined, the Pd atoms formed low-nuclearity Pd clusters on the In oxide surface. These catalysts showed higher activity compared to the dry-impregnation counterpart.

# 1.7 Aim of the project

The primary objective of this thesis was to obtain a more in-depth understanding of the influence of two core parameters on the In<sub>2</sub>O<sub>3</sub> activity for CO<sub>2</sub> hydrogenation to CH<sub>3</sub>OH: the catalyst composition and its preparation method. 11 different catalysts were synthetized by 5 different preparation methods and 3 possible compositions, and this thesis work attempted to find a clear trend correlated to these two crucial parameters.

The compositions consisted of the sole In<sub>2</sub>O<sub>3</sub>, the mixed oxide (molar ratio 1:1), and In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub>-Pd (with 0.25, 0.50, and 1.0 wt.% of Pd loading). We aimed to the comparison of the bulk oxide with its counterpart supported on ZrO<sub>2</sub>, to detect any influence of zirconia; and the comparison of the mixed oxide In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> with the equivalent In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub>-Pd, to establish the noble metal promoter effect on the activity. All the catalysts were synthetized with a one-pot method between urea combustion, urea hydrolysis, and coprecipitation with three different precipitating agents, i.e.: NH<sub>4</sub>OH, Na<sub>2</sub>CO<sub>3</sub>, and Na<sub>2</sub>C<sub>2</sub>O<sub>4</sub>.

The catalyst's physicochemical properties, such as phase, morphology, superficial characteristics, and redox properties, were investigated by the use of multiple characterization techniques. The catalysts were then tested for CO<sub>2</sub> hydrogenation reaction under the same reactor conditions and, ultimately, the spent catalysts were characterized after the catalytic test to identify any detectable change in their nature.

# 2. Methods

### 2.1 Chemicals

All chemicals used for catalyst preparation were  $In(NO_3)_3 \cdot xH_2O$  ( $\geq 99.99\%$ , Alfa Aesar),  $ZrO(NO_3)_2 \cdot yH_2O$  ( $\geq 99\%$ , Sigma-Aldrich),  $Pd(NO_3)_2$  solution (10% w/w (Pd content), Alfa Aesar), NH<sub>4</sub>OH solution (25%, VWR Chemical), urea ( $\geq 99.5\%$ , Sigma-Aldrich), Na<sub>2</sub>CO<sub>3</sub> ( $\geq 99.5\%$ , Sigma-Aldrich), Na<sub>2</sub>C<sub>2</sub>O<sub>4</sub> ( $\geq 99.5\%$ , Sigma-Aldrich), absolute ethanol (VWR Chemical), NaOH ( $\geq 99\%$ , VWR Chemical), Cu(NO<sub>3</sub>)<sub>2</sub>·3H<sub>2</sub>O (99-104 %, Sigma-Aldrich), Zn(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O ( $\geq 99\%$ , Sigma-Aldrich), Al(NO<sub>3</sub>)<sub>3</sub>·9H<sub>2</sub>O ( $\geq 98\%$ , Sigma-Aldrich), and MilliQ water (MILLIPORE, Direct-Q 3 UV).

Thermogravimetric analysis (TGA) was used to determine the water content in the  $In(NO_3)_3 \cdot xH_2O$  and  $ZrO(NO_3)_2 \cdot yH_2O$  precursors (Figure 10). The values for x and y were found to be 3.2 and 6.0, respectively.

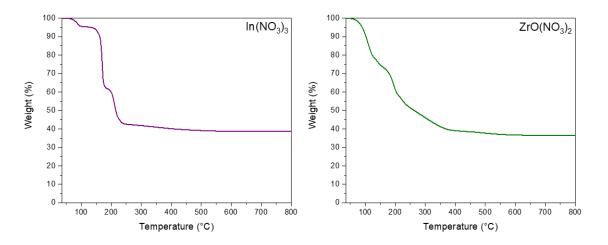


Figure 10 Weight loss profiles of the hydrate nitrate precursors of  $In(NO_3)_3 \cdot xH_2O$  (left) and  $ZrO(NO_3)_2 \cdot yH_2O$  (right) from TGA analysis.

# 2.2 Catalyst preparation

The synthesis protocol was designed to obtain about 4 g of each catalyst containing sole  $In_2O_3$  and mixed oxides of  $In_2O_3$ - $ZrO_2$  (molar ratio 1:1), or  $In_2O_3$ - $ZrO_2$ -Pd (with 0.25, 0.50, and 1.0 wt.% of Pd loading). The following synthesis methods were used: urea combustion, urea hydrolysis, and coprecipitation with three different precipitating agents, i.e.: NH<sub>4</sub>OH, Na<sub>2</sub>CO<sub>3</sub>, and Na<sub>2</sub>C<sub>2</sub>O<sub>4</sub>.

All the samples, with the only exception of the benchmark catalyst, were calcined under the same conditions: a temperature ramp from 20 to 500 °C with a heating rate of 5 °C min<sup>-1</sup> and a calcination plateau at 500 °C for 6 h. The benchmark catalyst was calcined at 400 °C (heating rate 5 °C min<sup>-1</sup>) for 6 h.

Table 2 displays the label assigned to each catalyst, according to their chemical composition and preparation method.

Acronym name	Composition	Preparation method
I-comb	In <sub>2</sub> O <sub>3</sub>	Urea combustion
I-ammo	In <sub>2</sub> O <sub>3</sub>	NH <sub>4</sub> /EtOH precipitation
I-hydro	In <sub>2</sub> O <sub>3</sub>	Urea hydrolysis
IZ-comb	In <sub>2</sub> O <sub>3</sub> -ZrO <sub>2</sub>	Urea combustion
IZ-ammo	In <sub>2</sub> O <sub>3</sub> -ZrO <sub>2</sub>	NH <sub>4</sub> /EtOH precipitation
IZ-hydro	In <sub>2</sub> O <sub>3</sub> -ZrO <sub>2</sub>	Urea hydrolysis
IZ-carb	In <sub>2</sub> O <sub>3</sub> -ZrO <sub>2</sub>	Na <sub>2</sub> CO <sub>3</sub> precipitation
IZ-oxa	In <sub>2</sub> O <sub>3</sub> -ZrO <sub>2</sub>	Na <sub>2</sub> C <sub>2</sub> O <sub>4</sub> precipitation
IZP-0.25	In <sub>2</sub> O <sub>3</sub> -ZrO <sub>2</sub> -Pd (0.25 wt.%)	Urea hydrolysis
IZP-0.50	In <sub>2</sub> O <sub>3</sub> -ZrO <sub>2</sub> -Pd (0.50 wt.%)	Urea hydrolysis
IZP-1.0	In <sub>2</sub> O <sub>3</sub> -ZrO <sub>2</sub> -Pd (1.0 wt.%)	Urea hydrolysis
CZA-bench	CuO-ZnO-Al <sub>2</sub> O <sub>3</sub>	Na <sub>2</sub> CO <sub>3</sub> /NaOH precipitation

Table 2 Information on catalyst labels, composition, and the preparation methods

# **2.2.1** Urea combustion (SCS method)

In the pure  $In_2O_3$  catalyst synthesis, 10.23 g  $In(NO_3)_3 \cdot xH_2O$  and 8.65 g of urea were mixed with a minimum amount of Milli-Q water in a ceramic crucible and kept under stirring for 1 h. The ratio between urea and indium nitrate precursor corresponded to the fuel to oxidizer ratio  $(\varphi)$  of 2,  $^{84}$  according to the reactions (5) and (6) stoichiometry:

(5) 
$$2 \text{ In}(NO_3)_3 + 5\varphi \text{ CH}_4N_2O + (\varphi - 1) O_2 \Rightarrow \text{In}_2O_3 + (5\varphi + 3) N_2 + (3.2 + 10\varphi) H_2O + 5\varphi CO_2$$

(6) 
$$2 \text{ ZrO(NO}_3)_2 + 5\phi/3 \text{ CH}_4\text{N}_2\text{O} + (\phi - 1) \text{ O}_2 \rightarrow \text{ZrO}_2 + (5\phi/3 + 1) \text{ N}_2 + (6 + 10\phi/3) \text{ H}_2\text{O} + 5\phi/3 \text{ CO}_2$$

After that, the crucible was transferred into an oven and the temperature was increased from 20 to 500 °C (heating rate of 5 °C min<sup>-1</sup>) and held at 500 °C for 6 h. This heating method is commonly known as "volume combustion".

This method yields a yellowish In<sub>2</sub>O<sub>3</sub> product in a form of light, fragile and foamy solid (Figure 11). The catalyst was denoted as *I-comb*, where "I" stands for In<sub>2</sub>O<sub>3</sub> and "comb" stands for the combustion method.



Figure 11 Image of  $In_2O_3$  material obtained by the combustion method (heating from 20 to 500 °C, followed by a 6 h plateau at 500 °C, a temperature ramp of 5 °C/min).

The mixed oxide  $In_2O_3$ - $ZrO_2$  was synthesized with the same protocol, using 7.08 g of  $In(NO_3)_3$ · $xH_2O$ , 3.39 g of  $ZrO(NO_3)_2$ · $yH_2O$ , and 7.99 g of urea. The catalyst was denoted as IZ-comb, where "IZ" stands for  $In_2O_3$ - $ZrO_2$ .

# 2.2.2 Urea hydrolysis

In a typical synthesis, 10.23 g In(NO<sub>3</sub>)<sub>3</sub>·xH<sub>2</sub>O and 25.96 g of urea were mixed with 150 mL of Milli-Q water in a round bottom flask and kept under stirring for 30 min. The flask was then placed in a sand bath at 90 °C for 16 h. The top part of the flask was connected with a reflux system using cold water to condense the water vaporized from the solution (Figure 12).

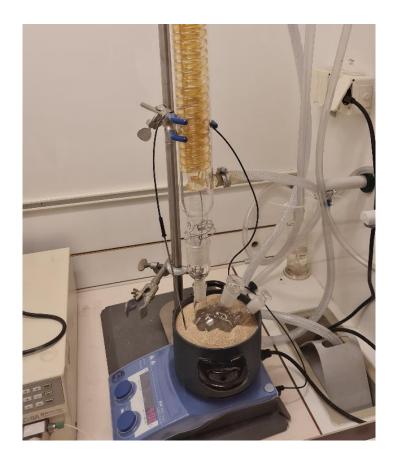


Figure 12 Urea hydrolysis method setup.

The final milky suspension was centrifugated and washed several times with a total of 1 L of distilled water. The solid product was dried at 80 °C for 16 h and subsequently calcined at 500 °C for 6 h (heating rate 5 °C min<sup>-1</sup>). The catalyst was denoted as *I-hydro*, where "hydro" stands for the urea hydrolysis method.

A mixed oxide of In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> catalyst was prepared with a similar protocol using 7.08 g of In(NO<sub>3</sub>)<sub>3</sub>·xH<sub>2</sub>O, 3.39 g of ZrO(NO<sub>3</sub>)<sub>2</sub>·yH<sub>2</sub>O, and 29.97 g of urea. This catalyst was denoted as *IZ-hydro*.

In addition, three samples containing different loadings of Pd (0.25 wt.%, 0.50 wt.%, 1.0 wt.%) were also prepared using the same protocol as *IZ-hydro* but given amounts of the Pd(NO<sub>3</sub>)<sub>2</sub> precursor was added into the solutions before the heating step. The three catalysts containing Pd were labeled as IZP-0.25 (0.25 wt.%), IZP-0.50 (0.50 wt.%), and IZP-1.0 (1.0 wt.%), where "IZP" stands for In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub>-Pd and the numbers stand for the weight loading of Pd in the catalysts. The preparation method is not stated, because the only Pd-containing catalysts were synthesized with the urea hydrolysis method.

# 2.2.3 Precipitation using NH<sub>4</sub>OH/EtOH solution

In a typical synthesis,<sup>41</sup> 10.23 g In(NO<sub>3</sub>)<sub>3</sub>·xH<sub>2</sub>O was dissolved in 150 mL of Milli-Q water in a beaker and kept under stirring for 30 min. Then, a mixture of NH<sub>4</sub>OH solution (25% in water) and absolute ethanol (volume ratio 1:2) was added dropwise into the In(NO<sub>3</sub>)<sub>3</sub> solution until the pH reached around 9.2. The milky solution was kept under stirring for 30 min and then it was aged at 80 °C for another 30 min. Finally, the solution was centrifugated and washed with 1 L of water. The solid product was dried at 80 °C for 16 h and subsequently calcined at 500 °C for 6 h (heating rate 5 °C min<sup>-1</sup>). The catalyst was denoted as *I-ammo*, where "ammo" stands for the employment of an ammonia solution.

A mixed oxide of  $In_2O_3$ - $ZrO_2$  was synthesized in a similar protocol using 7.08 g of  $In(NO_3)_3$ ·xH<sub>2</sub>O and 3.39 g of  $ZrO(NO_3)_2$ ·yH<sub>2</sub>O. The catalyst was labeled as IZ-ammo.

# 2.2.4 Precipitation using Na<sub>2</sub>CO<sub>3</sub>

One sample containing mixed oxide of In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> was prepared using 7.08 g of In(NO<sub>3</sub>)<sub>3</sub>·xH<sub>2</sub>O and 3.39 g of ZrO(NO<sub>3</sub>)<sub>2</sub>·yH<sub>2</sub>O. The same procedure of the NH<sub>4</sub>OH/EtOH precipitation was followed, however, a solution of Na<sub>2</sub>CO<sub>3</sub> 1 M was used as a precipitating agent to replace the mixture of NH<sub>4</sub>OH/EtOH solution. The resulting mixture was aged at room temperature for 30 min. After that, the suspension was centrifugated and washed with 4 L of hot water (80 °C), until neutral pH, to remove Na as much as possible. The catalyst was labeled *IZ-carb*, where "carb" stands for the use of carbonate as a precipitating agent.

# 2.2.5 Precipitation using Na<sub>2</sub>C<sub>2</sub>O<sub>4</sub>/NaOH

One sample of a mixed oxide of In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> was prepared using 7.08 g of In(NO<sub>3</sub>)<sub>3</sub>·xH<sub>2</sub>O and 3.39 g of ZrO(NO<sub>3</sub>)<sub>2</sub>·yH<sub>2</sub>O, similarly to the case of the precipitation using Na<sub>2</sub>CO<sub>3</sub>; however, a solution of Na<sub>2</sub>C<sub>2</sub>O<sub>4</sub> 0.3 M was used as a precipitating agent.<sup>85</sup> Note that the pH reached a plateau under the desired amount, with the addition of sodium oxalate. Therefore, it was necessary to add 25 mL of 3 M NaOH solution to reach the 9.2 pH during the precipitation. After a 30 min aging at room temperature, the suspension was filtered and washed with 4 L of hot water (80 °C) to remove Na as much as possible.

# 2.2.6 Benchmark catalyst CuZnAl

A benchmark catalyst containing mixed oxides of Cu, Zn, Al with a nominal molar ratio of Cu/Zn/Al = 60/30/10 was prepared by the coprecipitation method. Along A nitrate solution (1.0 M, 65 mL) containing Cu/Zn/Al = 60/30/10 (molar ratio) was added dropwise into a beaker containing Na<sub>2</sub>CO<sub>3</sub> solution (0.5 M, 26 mL) at 20 °C under stirring with a magnetic stirrer at 500 rpm. The pH was adjusted at  $8.0 \pm 0.1$  by the addition of a solution of NaOH (3.0 M). Note that the amount of Na<sub>2</sub>CO<sub>3</sub> was based on the charge balance of the hydrotalcite-like formulation when substituting a divalent cation (Cu<sup>2+</sup> and Zn<sup>2+</sup>) in the brucite structure with a trivalent cation (Al<sup>3+</sup>) with an excess amount of 4-fold. The resulting suspension was aged for 2 h at 20 °C and subsequently filtered and washed with hot water (80 °C, 1.2 L) until neutral pH. The solid was dried at 60 °C for 24 h and it was then ground into a fine powder using a mortar. After that, the material was calcined at 400 °C (heating rate 5 °C min<sup>-1</sup>) for 6 h. The catalyst was denoted as CZA-bench.

### 2.3 Characterization

# 2.3.1 Elemental analysis

Elemental compositions of the catalysts were analyzed using Inductively Coupled Plasma Sector Field Mass Spectrometry (ICP-SFMS).

The ICP-MS is a type of mass spectroscopy that uses inductively coupled plasma, electromagnetically produced, to atomize the sample forming atomic and polyatomic ions, which are then detected by the mass spectrometer.<sup>87</sup>

The measurements were performed by ALS Scandinavia (Luleå, Sweden).

# 2.3.2 X-ray diffraction (XRD)

X-ray diffraction (XRD) is a non-destructive analysis employed to analyze the structure of crystalline solid materials. X-rays are generated from a source, filtered to obtain monochromatic radiation, and radiate it at the sample (Figure 13). The X-rays can interact with the sample in various ways, but this analysis goes in search of constructive interference of the X-rays scattered from the sample, following Bragg's Law (Equation 1):

#### $n \lambda = 2d \sin\theta$

This law relates the wavelength of the incident electromagnetic radiation ( $\lambda$ ) to the diffraction angle ( $\theta$ ) and the lattice spacing in a crystalline sample (d); n is the reflection order, which will always be an integer. The diffracted X-rays are detected by scanning the sample through a range of  $2\theta$  angles. Interpreting the diffraction pattern can give useful information, such as the sample's crystalline phases, the amount of amorphous solid, and the crystallites dimension; but the pattern reading can only be achieved by comparison of the above with standard reference patterns (e.g., Powder Diffraction Files, or PDFs). <sup>88</sup>

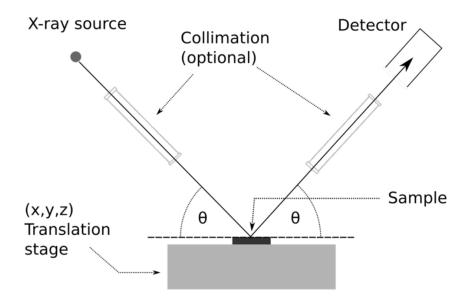


Figure 13 Schematic of an X-ray diffractometer.89

XRD measurements were performed for the fine powder of the catalysts using a D8 Advance Diffractometer (Bruker AXS, Germany). The diffractograms were recorded from  $10^{\circ}$  to  $70^{\circ}$  (20) with a step size of  $0.02^{\circ}$  (1 s per step). The X-ray source employed was a copper anode.

The average crystallite sizes of  $In_2O_3$  denoted  $d_c$ , were determined using the Scherrer equation (Equation 2), where  $\beta$  is the full width at half maximum (FWHM) and the Bragg angles  $\theta$  at  $In_2O_3$  (431) reflection (2 $\theta$  around 45.5°) were determined from the XRD pattern. The wavelength  $\lambda$  of the  $CuK_\alpha$  and the shape factor  $K_F$  were 0.15406 nm and 0.89, respectively.

Equation 2

$$d_c = \frac{K_F \lambda}{\beta \cos \theta}.$$

# 2.3.3 Scanning electronic microscopy (SEM) and Energy-Dispersive X-ray (EDX)

SEM is a type of electron microscopy that produces three-dimensional images from the detection of an electron beam that interacted with the atoms in the sample, permitting a high scanning resolution. From an SEM instrument information on topography and composition can be drawn.

When the intense primary electron beam hits the sample, numerous interactions can happen (Figure 14) between the electrons and the atoms in the sample. Most of the time, the SEM instrument detects Secondary Electrons (SEs), generated as the products of the sample ionization, by the primary electrons. SEs are highly localized and they only escape from the upper surface of the sample, thus allowing to obtain the surface three-dimensional image by combining the position of the secondary beams and their intensity.

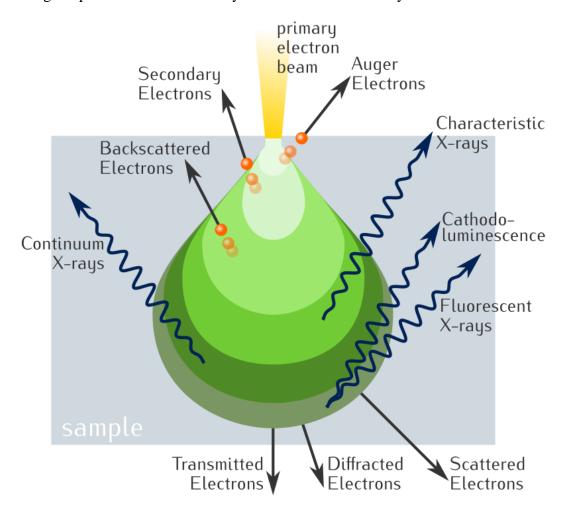


Figure 14 Electron-matter interaction depth and type of signal generated. 90

The energy released after the ionization of the sample can cause the production of the so-called characteristic X-rays (Figure 14), specific for every element. Through the use of these, we can

carry out an overall or a regional EDX scan to detect the morphological composition of the sample.<sup>91</sup>

SEM was used to investigate the morphology of the catalysts. High-resolution images were acquired using JEOL JSM-7800F Prime instrument equipped with an EDX (energy-dispersive X-ray) detector and an SXES (Soft X-ray emission spectrometer).

## 2.3.4 Nitrogen adsorption/desorption at -196 °C

The N<sub>2</sub> adsorption-desorption analysis is a common and simple method that investigates the surface properties of a solid, such as its Specific Surface Area (SA), Pore Size Distribution, the total volume of the pores, and the type of porosity, by the employment of liquid N<sub>2</sub> at -196 °C (77 K). The solid's surface (adsorbate) adsorbs the N<sub>2</sub> molecules (adsorbate) through Van der Waals forces, and different adsorbate layers are formed (multilayers). The BET (Brunauer-Emmett-Teller) model<sup>92</sup> is applied to obtain the material surface area (Equation 3), and its complementary BJH (Barret-Joyner-Halenda) model is used to obtain the pores size distribution (PSD).

The surface adsorption capacity of molecular nitrogen in a solid surface depends on its relative pressure  $(P/P_0)$  where P is the partial pressure of nitrogen and  $P_0$  is the saturated vapor pressure of nitrogen under liquid  $N_2$  temperature. <sup>93</sup>

Equation 3

$$SA_{BET} = n_m^a * L * \sigma_m$$

Where  $n_m^a$  is the material's monolayer capacity [mol], L is the Avogadro's number [molecules mol<sup>-1</sup>] and  $\sigma_m$  is the  $N_2$  cross-sectional area [m<sup>2</sup> molecule<sup>-1</sup>].

The scheme of a typical BET instrument is shown in Figure 15:

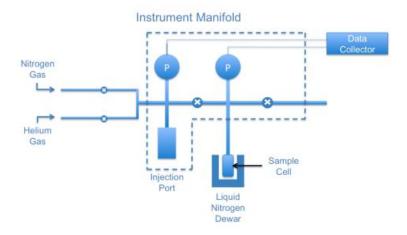


Figure 15 Schematic representation of an N<sub>2</sub> adsorption-desorption instrument.

The textural properties of the catalysts were investigated with nitrogen physisorption. The measurements were performed at -196 °C (77 K) using a Micromeritics Tristar instrument. In a typical measurement, approximately 0.2 g of powder catalyst was pre-treated at 250 °C for 8 h. The specific surface area ( $S_{BET}$ ) was calculated using the Brunauer-Emmett-Teller (BET) multiple-point method in the relative pressure range p/p<sub>0</sub> from 0.05 to 0.3. The total pore volume ( $V_p$ ) was calculated at p/p<sub>0</sub> = 0.97.

#### 2.3.5 X-ray photoelectron spectroscopy (XPS)

XPS is a spectroscopy technique that studies the surface characteristics of a specimen by the employment of the photoelectric effect: the emission of electrons when electromagnetic radiation hits a material; as represented in Figure 16 when the electromagnetic radiation hits a surface, and its photons have higher energy than the material's electrons binding energy, the latter are ejected as characteristic photons. The electromagnetic radiation's wavelength used for this analysis is in the X-ray part of the spectra. This technique can provide qualitative and quantitative information about the surface of a material, such as the elemental composition and the chemical states of elements and chemical surroundings.<sup>94</sup>

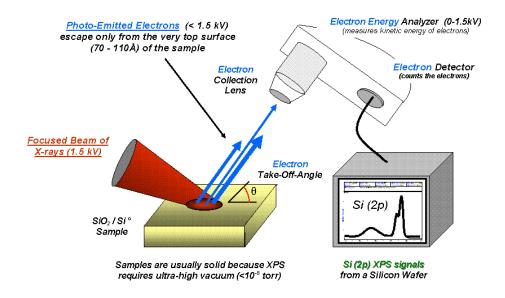


Figure 16 Schematic representations of a monochromatic XPS system. 95

The oxidation states of each element of the catalyst were determined with XPS. The measurements were performed using a Perkin-Elmer PHI 5000 VersaProbe III – Scanning XPS Mircoprobe<sup>TM</sup> apparatus (X-ray source AlK $_{\alpha}$  radiation with energy 1486.6 eV). The binding energy of C1s at 284.8 eV was used to calibrate the system before performing narrow scan measurements.

# 2.3.6 Temperature-programmed desorption with $CO_2$ ( $CO_2$ -TPD) and $O_2$ ( $O_2$ -TPD)

Temperature Programmed Desorption (TPD) is a characterization method used to study the surface adsorption features of a material, by employing specific gaseous carry molecules to investigate characteristic adsorption sites (basic or acid sites, O-vacancies, ...). The solid is first scrubbed with an inert gas at high temperatures to remove any previous adsorbate (H<sub>2</sub>O, CO<sub>2</sub>, ...), to then be saturated with the probe molecule of interest; at this point, a constant temperature gradient is applied to desorb at a characteristic temperature according to the adsorption strength, the desorbed probe molecules that are detected through a mass spectrometer (MS). In this thesis, the probe molecules that have been studied were CO<sub>2</sub> and O<sub>2</sub> to study, respectively, CO<sub>2</sub>-adsorption sites of various nature and O-vacancies present in the catalyst surface. <sup>96</sup>

CO<sub>2</sub>-TPD and O<sub>2</sub>-TPD measurements were performed using a calorimeter (Sensys DSC, SETARAM instrumentation) coupled with a mass spectrometer (HPR-20 QIC, Hidden analytical). The sieved catalyst (approximately 50 mg for CO<sub>2</sub>-TPD and 30 mg for O<sub>2</sub>-TPD, with a particle size of  $180-250 \,\mu m$ ) was loaded in a quartz fixed-bed reactor (inner diameter 4 mm).

#### 2.3.6.1 CO<sub>2</sub>-TPD

The catalyst was pre-treated at 300 °C for 30 min (temperature ramp 5 °C min<sup>-1</sup>) in Ar (20 mL min<sup>-1</sup>) and then cooled to 25 °C. A flow of 20 mL min<sup>-1</sup> of 5000 ppm  $CO_2/Ar$  was then introduced to the reactor for 1 h in the adsorption step. After that, the reactor was purged with 20 mL min<sup>-1</sup> of Ar for 30 min to remove the weak adsorbed  $CO_2$ . The temperature was subsequently ramped from 25 to 700 °C (with a rate of 10 °C min<sup>-1</sup>) and held at 700 °C for 15 min in Ar flow.  $CO_2$  was tracked by a mass number m/z = 44.

#### 2.3.6.2 O<sub>2</sub>-TPD

O<sub>2</sub>-TPD measurements were performed in a similar procedure as CO<sub>2</sub>-TPD, except for the adsorption step a flow of 20 mL min<sup>-1</sup> of 2500 ppm O<sub>2</sub>/Ar was used instead of CO<sub>2</sub>. In the desorption step, the temperature was ramped from 25 to 800 °C (with a rate of 10 °C min<sup>-1</sup>) and held at 800 °C for 15 min in Ar flow. O<sub>2</sub> was tracked by a mass number m/z = 32.

#### 2.3.7 Temperature-programmed reduction with H<sub>2</sub> (H<sub>2</sub>-TPR)

The H<sub>2</sub>-Temperature Programmed Reduction (H<sub>2</sub>-TPR) is employed to investigate the redox properties of a material's surface and its apparatus works similarly to the TPD one: after a preliminary scrub, H<sub>2</sub> is introduced in the line, and the temperature is then ramped with a constant temperature gradient; in this analysis, though, adsorption does not play a role and the signal detected is not the carry molecule desorbed, but the H<sub>2</sub> consumption by the solid, therefore, a negative signal.<sup>97</sup>

H<sub>2</sub>-TPR measurements were performed using the same instrument setup as CO<sub>2</sub>-TPD and O<sub>2</sub>-TPD. Approximately 20 mg of the catalyst was pre-treated at 300 °C for 30 min (temperature

ramp 5 °C min<sup>-1</sup>) in Ar (20 mL min<sup>-1</sup>) and then cooled to 25 °C. A flow of 20 mL min<sup>-1</sup> of 1 vol.% H<sub>2</sub>/Ar was then introduced to the reactor for 30 min at 25 °C. After that, the temperature was subsequently ramped from 25 to 800 °C (with a rate of 10 °C min<sup>-1</sup>) and held at 800 °C for 15 min in Ar flow. H<sub>2</sub> was tracked by the mass number m/z = 2.

#### 2.3.8 CO chemisorption

Pd dispersions in the Pd-containing catalysts were determined with CO chemisorption using an ASAP2020 Plus instrument (Micromeritics). Approximately 0.1 g of catalyst (180 – 250 µm particle size) was loaded in a U-shape quartz reactor and then pre-treated in He, evacuated in vacuum at 110 °C, and reduced in H<sub>2</sub> at 400 °C for 1 h. The reactor was subsequently evacuated to 5 µmHg at 400 °C for 30 min and cooled to 35 °C. After that, the reactor was further evacuated to 5 µmHg at 35 °C and a leak test was performed. The sample was again evacuated to 5 µmHg. The first adsorption isotherm (total isotherm) was performed in the pressure range from 100 to 600 mmHg (interval of 25 mmHg). After the first isotherm was completed, the reactor was evacuated to remove physically adsorbed CO before the second adsorption isotherm was repeated. The isotherm of chemisorbed CO was obtained by subtracting the difference between the two isotherms. The intercept of a linear regression curve fit from the isotherm of chemisorbed CO was attributed to the amount of adsorbed CO on a monolayer of the metal surface. The dispersion was calculated with Equation 4:

Equation 4

$$D_{\rm M}(\%) = \frac{F_S N_{CO}}{N_{\rm M}}.100$$

where  $N_M$  is the total number of atoms of metal,  $N_{CO}$  is the number of CO molecules adsorbed on the monolayer, and  $F_s$  is a stoichiometric factor considering the form of CO adsorption on the metal. The stoichiometry factor was 2 for Pd. <sup>99</sup> The crystallite size was reported based on the assumption of hemispheric particles.

## 2.4 Catalytic tests

The CO<sub>2</sub> hydrogenation to methanol was performed in a pressurized, continuous-flow, and fixed-bed tubular stainless-steel reactor (VINCI Technologies, France), with an inner diameter of 1.27 cm and length of 21.5 cm. The reactor total volume was 12.1 cm<sup>3</sup> and it was vertically positioned, with a thermocouple attached to its bottom that ran up to the center (Figure 17).

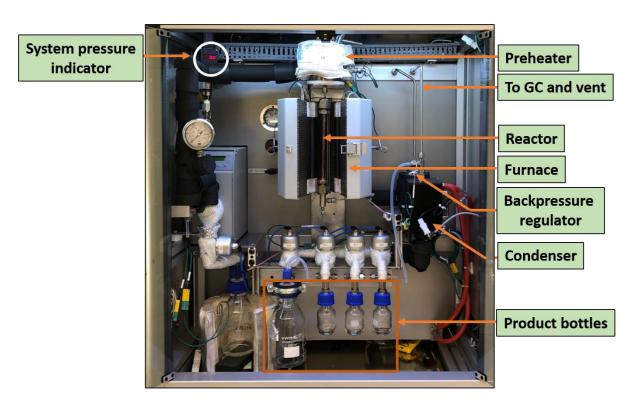


Figure 17 Reactor's apparatus.

All catalysts were pelletized and a fraction of particle size between 250 and 500  $\mu$ m was collected and used for the activity tests to avoid the pressure drop issue. For comparison purposes, the activity tests were designed by keeping the same amount of In metal (500 mg) in each sample. This required 605 mg of In<sub>2</sub>O<sub>3</sub>, 873 mg of In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> and in the case of Pd-containing catalysts, it was 875 mg, 877 mg, and 882 mg of In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub>-Pd 0.25 wt.%, 0.50 wt.%, and 1.0 wt.%, respectively. In this way, all tests had the same Weight Hourly Space Velocity (WHSV) of 12000 mL  $g_{In}^{-1}$  h<sup>-1</sup>.

Regarding the reference catalyst CuO-ZnO- $Al_2O_3$ , the total amount of metal (Cu, Zn, and Al) was kept the same as in the In-based catalysts (4.35 mmol g<sup>-1</sup> which correspond to 336 mg of the reference catalyst).<sup>72</sup>

The catalyst was packed inside the reactor at the vertical center position of the reactor such that the bottom thermocouple tip was in contact with the catalyst bed and the remaining portions of the reactor were filled with SiC (500  $\mu$ m size particles). For easy separation, the catalytic bed was placed between two thin layers of quartz wool both upstream and downstream so that the catalytic bed was separated from the extra-filling portions of SiC.

#### 2.4.1 Pre-treatment and running conditions

The reactor was placed inside a furnace. H<sub>2</sub> and CO<sub>2</sub> were fed through separate mass flow controllers upstream from the reactor.

After a leak test at 40 bars, the catalyst was pre-treated by heating from room temperature to 350 °C (with a ramp of 5 °C min<sup>-1</sup>) and maintained at 350 °C for 1 h in Ar flow of 150 NmL min<sup>-1</sup>. The feed gas was then switched to a mixture of 25 NmL min<sup>-1</sup> of CO<sub>2</sub> and 75 NmL min<sup>-1</sup> of H<sub>2</sub> (molar ratio of CO<sub>2</sub>:H<sub>2</sub> = 1:3) and the reactor was pressurized to 40 bars. The catalytic tests were conducted at five temperatures from 250 to 350 °C (interval step of 25 °C) at Weight Hourly Space Velocity (WHSV) of 12000 mL  $g_{In}^{-1}$  h<sup>-1</sup>.

The reference catalyst CuO-ZnO-Al<sub>2</sub>O<sub>3</sub> was tested under the same condition, except it was reduced with a flow of 5% H<sub>2</sub>/Ar before doing the catalytic test.<sup>42</sup>

Immediately downstream from the reactor, a back pressure regulating valve was installed near the exit of the reactor to reduce the pressure of the effluent gas to near atmospheric pressure before it flowed into a condenser at room temperature.

The effluent gas from the reactor was quantitatively analyzed online using a gas chromatograph (GC, SCION 456) equipped with both thermal conductivity (TCD) and flame ionization detectors (FID). The FID data was not taken into consideration in this thesis work. The GC was calibrated with varying concentrations of absolute methanol, CO<sub>2</sub>, CO, and CH<sub>4</sub>. All calculations were performed with the data collected after the steady-state conditions were reached, obtained in approximately 50 minutes.

#### 2.4.2 Parameters

Carbon balances were all greater than 95 % for all experiments.  $CO_2$  conversion ( $X_{CO2}$ ) was calculated based on the molar flow rates as:

Equation 5

$$X_{CO_2} = \frac{F_{CO_2,in} - F_{CO_2,out}}{F_{CO_2,in}} \times 100 \%$$

where F<sub>CO2, in</sub> and F<sub>CO2, out</sub> are the molar CO<sub>2</sub> flow rates at the inlet and outlet respectively.

The selectivities to methanol ( $S_{CH3OH}$ ) and its side products CO ( $S_{CO}$ ) and CH<sub>4</sub> ( $S_{CH4}$ ) are calculated as follows:

Equation 6

$$S_{CH_3OH} = \frac{F_{CH_3OH,out}}{F_{CO_2,in} - F_{CO_2,out}} \times 100 \%$$

Equation 7

$$S_{CO} = \frac{F_{CO,out}}{F_{CO_2,in} - F_{CO_2,out}} \times 100 \%$$

Equation 8

$$S_{CH_4} = \frac{F_{CH_4 \ out}}{F_{CO_2,in} - F_{CO_2,out}} \times 100 \%$$

where  $F_{CH3OH,out}$ ,  $F_{CO,out}$ , and  $F_{CH4,out}$  are the corresponding outlet molar flow rates of methanol, CO, and CH<sub>4</sub> respectively.

## 3. Result and discussions

## 3.1 Compositional study

#### 3.1.1 Elemental analysis through Inductively Coupled Plasma (ICP)

For each catalyst, the theoretical amount of calcined material was aimed to be 4 g. All synthesis methods provided approximately 3.7 – 3.9 g of the products (92.5-97.5% yields) except for the two samples synthesized by the urea combustion method (ca. 2.2 g and 55% yield). A significant loss in yield of the products prepared by the combustion method did not allow interpreting the elemental composition of these products. Therefore, elemental analysis was conducted by using Inductively Coupled Plasma (ICP) Spectroscopy to verify the compositions of the samples prepared by the combustion method as well as the Pd contents of the IZP series and the possible presence of trace Na in the IZ-carb and IZ-oxa which used Na-containing precipitating agents.

Table 3 Inductively Coupled Plasma (ICP) analysis results for the  $In_2O_3$ - $ZrO_2$  and  $In_2O_3$ - $ZrO_2$ -Pd catalysts series.

	In molar %	Zr molar %	Pd wt.%	ppm Na
IZ-comb	48.23	51.77		
IZ-hydro	66.11	33.89		
IZ-ammo	64.91	35.09		
IZ-carb	66.98	33.02		<50
IZ-oxa	65.21	34.79		<50
IZP-0.25	64.78	35.22	0.07	
IZP-0.50	65.82	34.18	0.14	
IZP-1.0	66.6	33.4	0.23	
Theoretical values	66.67	33.33		

As shown in Table 3, all the catalysts showed a molar ratio of In:Zr of approximately 2:1 which is close to the expected value ( $In_2O_3$ : $ZrO_2$  of 1:1 or In:Zr of 2:1), except for the IZ-comb which had a molar ratio of In:Zr = 1:1. A significantly lower ratio of In:Zr indicates that Indium was clearly lost during the combustion process during the synthesis of IZ-comb and most probably I-comb, which showed the same weight loss after the synthesis. This is perhaps due to the loss of Indium precursor, e.g., in the vent line after the ignition during the combustion process.

The Pd contents were 0.07, 0.14 and 0.23 wt.% for IZP-0.25, IZP-0.5, and IZP-1.0 (Table 3), respectively. These values were significantly lower than the expected values, of around four times. The urea hydrolysis synthesis method involves the slow urea hydrolysis that carries the pH solution to higher values thanks to the NH<sub>4</sub>OH production, together with CO<sub>2</sub>. The reason for this unexpected Pd content is most probably the formation of a stable and water-soluble complex of Pd and ammonia ( $[Pd(NH_3)_4]^{2+}$ ) that has a high stability constant ( $\beta \approx 10^{33}$ ) in the alkaline environment containing ammonia, <sup>100</sup> and that suppressed partially the complete precipitation of Pd(OH)<sub>2</sub> in the mixed hydroxides. However, the correlation of the nominal and actual values for the Pd content is linear, suggesting that the Pd content could be controlled with this synthesis method, but not without a partial loss of Pd.

The Na contents of the two samples IZ-carb and IZ-oxa, synthesized using Na-containing precipitating agents, were below the Limit Of Detection (LOD) of the instrument employed (50 ppm) (Table 3). This indicates that post-synthesis washing is effective for Na removal, thus allowing us to compare the activity directly without the interference of Na, which is a potentially active species in the CO<sub>2</sub> hydrogenation reaction.<sup>101</sup>

## 3.1.2 CO chemisorption

CO chemisorption analysis was conducted for the three samples of the IZP series to determine the Pd dispersions. The results are shown in Table 4. The three catalysts had a Pd dispersion from 23 to 25%, corresponding to the particle sizes of approximately 5 nm. A very narrow range of Pd loadings (0.07 - 0.23 wt.%) resulted in a similar dispersion of Pd among three catalysts, therefore no substantial difference was detected.

*Table 4 CO chemisorption analysis results for the In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub>-Pd catalysts series.* 

	Dispersion (%)	Particle size (nm)
IZP-0.25	22.90	4.9
IZP-0.50	25.00	4.5
IZP-1.0	24.40	4.6

## 3.2 Phase study

#### 3.2.1 X-Ray Diffraction (XRD)

XRD measurements were performed to investigate the crystalline phases of the catalysts. The data were organized into three sets to have a better comparison of the impact of the preparation methods on the structure of the catalysts:

- 1. Three main preparation methods (comb, hydro, and ammo) for  $ZrO_2$  (Z),  $In_2O_3$  (I), and  $In_2O_3$ - $ZrO_2$  (IZ).
- 2. Five methods (comb, hydro, ammo, carb, and oxa) for the In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> (IZ) series.
- 3. The urea hydrolysis for the In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub>-Pd (IZP) series with different Pd loadings.

This 3-set grouping will be repurposed in the following paragraphs, for a good comparison for the 3 different series.

The crystallites sizes reported hereafter, were calculated with the Scherrer equation (Equation 2) using the input information of the plane (431) of  $In_2O_3$  at a 20 of 45.5°.

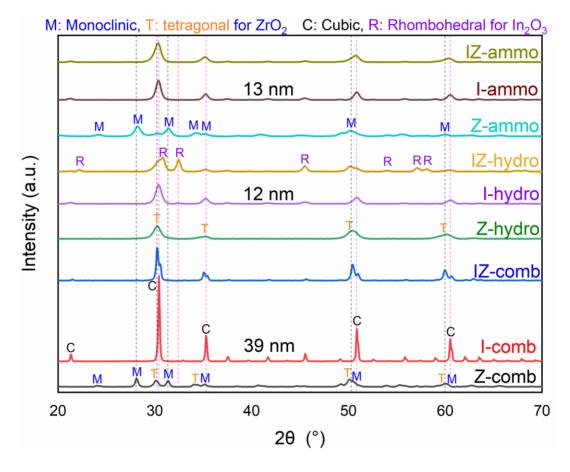


Figure 18 X-Ray Diffraction (XRD) patterns of ZrO<sub>2</sub>, In<sub>2</sub>O<sub>3</sub>, and In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> prepared by the urea combustion (comb), urea hydrolysis (hydro), and precipitation using ammonia solution (ammo).

Figure 18 presents the XRD patterns of ZrO<sub>2</sub>, In<sub>2</sub>O<sub>3</sub>, and In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> prepared by the urea combustion (comb), urea hydrolysis (hydro), and precipitation using ammonia solution (ammo). The reflections of a cubic structure (space group Ia-3 (206), PDF 00-006-0146) were found for three samples of In<sub>2</sub>O<sub>3</sub> regardless of the synthesis method. This structure has also been reported in the literature. However, the preparation method significantly influenced the crystalline sizes: the combustion method generated the In<sub>2</sub>O<sub>3</sub> with a crystallite size of 39 nm (I-comb), which was almost three-fold larger than those prepared by the urea hydrolysis (I-hydro, 12 nm) and precipitation with ammonia (I-ammo, 13 nm). In contrast with In<sub>2</sub>O<sub>3</sub>, the synthesis methods had a substantial impact on the structure of ZrO<sub>2</sub>. Z-hydro showed a tetragonal (T) phase (space group P42/nmc (137), PDF-00-065-0729);<sup>41</sup> while Z-ammo shows a monoclinic (M) phase (P21/a (14), PDF 00-065-0728);<sup>42,47</sup> Z-comb had a mixed phase of both T and M.

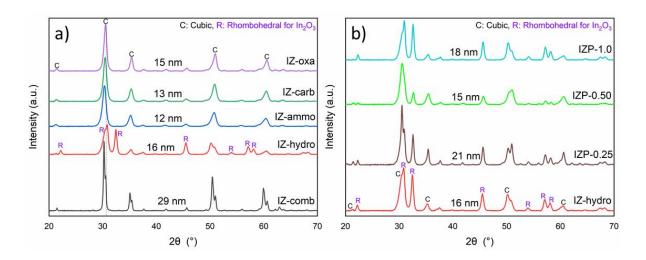


Figure 19 X-Ray Diffraction (XRD) patterns of (a) In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> series prepared by the urea combustion (comb), urea hydrolysis (hydro) and precipitation using ammonia solution (ammo), carbonate solution (carb), and oxalate solution (oxa); (b) XRD patterns of In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub>-Pd series prepared by urea hydrolysis (hydro) with different Pd loading (0.25, 0.50 and 1.0 wt.%).

For  $In_2O_3$ -  $ZrO_2$  catalysts (Figure 19a), IZ-ammo shows a solid solution of  $In_2O_3$  and  $ZrO_2$  with a cubic structure (like  $Zr_{0.18}In_{1.75}O_3$ , PDF 04-006-0768), or it could be that the reflections of  $ZrO_2$  masked the reflection of  $In_2O_3$ . This structure was also found in the IZ-hydro sample and IZ-carb, as well as IZ-oxa. However, the IZ-hydro catalyst also had a rhombohedral phase (also known as "hexagonal" phase in literature) of  $In_2O_3$  (PDF 04-001-8476). By contrast, the patterns of IZ-comb showed a mixture of both cubic phase of  $In_2O_3$  and tetragonal of  $ZrO_2$  without a solid solution. The effect of the synthesis methods on the crystallite sizes of  $In_2O_3$ - $ZrO_2$  catalysts was similar to  $In_2O_3$ . The IZ-comb showed the size of 29 nm whereas other samples had the particle size in a range of II of II.

Figure 19b presents the XRD patterns of the IZP catalysts. Three Pd-containing samples had both cubic phase of In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> and rhombohedral phase of In<sub>2</sub>O<sub>3</sub> which was similar to the structure of the IZ-hydro catalyst. This implied that the Pd presence did not modify the phase of the samples. However, the crystallite sizes of the Pd-containing samples were increased slightly to some extent with the IZ-hydro catalyst.

## 3.3 Morphology study

# 3.3.1 SEM (Scanning Electron Microscopy) and EDS (Energy-Dispersive X-ray Spectroscopy)

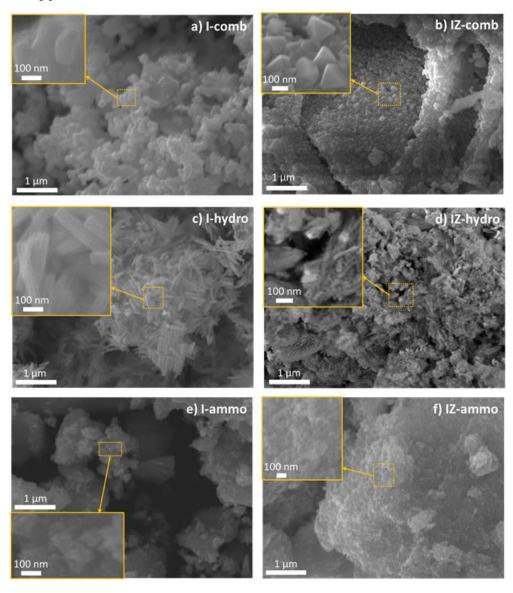


Figure 20 Scanning Electron Microscopy (SEM) images of In<sub>2</sub>O<sub>3</sub> and In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub>: (a) I-comb; (b) IZ-comb; (c) I-hydro; (d) IZ-hydro; (e) I-ammo; (f) IZ-ammo.

SEM measurements were performed to investigate the morphology of the catalysts. Figure 20 displays the SEM images of In<sub>2</sub>O<sub>3</sub> and In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> catalysts prepared by the combustion, urea hydrolysis, and precipitation using ammonia solution. The I-comb showed an agglomeration of small bended-grains, around 200 nm long (Figure 20a). This morphology was also found in the IZ-comb sample, together with well-defined tetragonal crystals (Figure 20b); these tetragonal crystals perhaps belonged to the tetragonal phase of ZrO<sub>2</sub>, which would be consistent with the XRD data as both cubic phase of In<sub>2</sub>O<sub>3</sub> and tetragonal ZrO<sub>2</sub> were identified in the XRD pattern of the IZ-comb. I-hydro showed rod particles with a length of roughly half of a micron (Figure 20c). The rod morphology was also partially observed in the IZ-hydro, together with a cluster non-well-defined structure (Figure 20d). Compared with the phase identified from XRD, it is hypothesized that the rod particles could be, perhaps, associated with the cubic structure of the solid solution of In<sub>2</sub>O<sub>3</sub> and ZrO<sub>2</sub> whereas the cluster morphology belonged to the hexagonal phase (rhombohedral). The I-ammo has a non-well-defined morphology, with big and compact clusters agglomeration (Figure 20e) whereas the IZ-ammo also showed a similar morphology but with smaller clusters (Figure 20f).

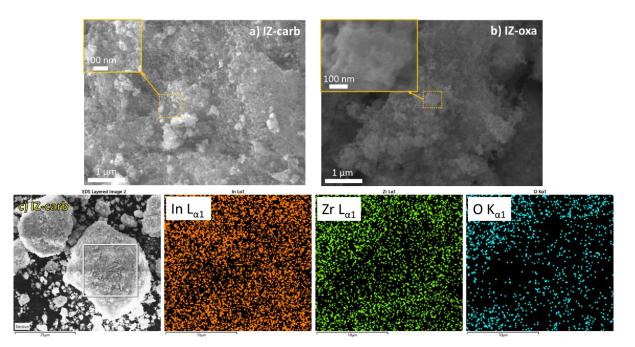


Figure 21 Scanning Electron Microscopy (SEM) images of In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> prepared by precipitation using (a) carbonate solution (carb) and (b) precipitation using oxalate solution (oxa). (c) Energy-Dispersive X-ray Spectroscopy (EDS) analysis of IZ-carb.

Both IZ-carb and IZ-oxa showed a similar morphology to the IZ-ammo (Figure 21a and Figure 21b).

Additionally, to analyze the element distribution and homogeneity in the IZ-carb sample, Energy-Dispersive X-ray Spectroscopy (EDS) analysis was performed and the elemental maps are displayed in Figure 21c: overlapped signals of In and Zr were observed, suggesting a homogeneous distribution in the area selected; this result coherently agrees with the XRD data in which a solid solution between Zr and In oxides was identified.

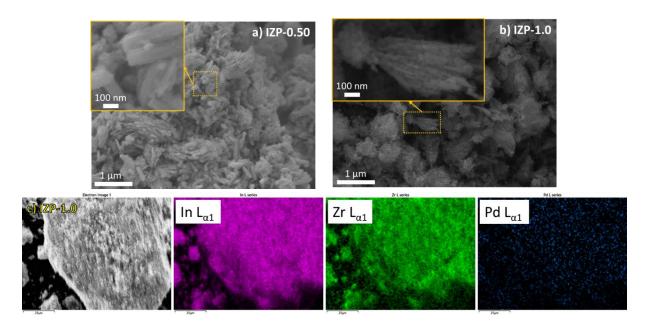


Figure 22 Scanning Electron Microscopy (SEM) images of In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub>-Pd prepared by urea hydrolysis (hydro) method with a Pd loading of (a) 0.50 wt.% and (b) 1.0 wt.%. (c) Energy-Dispersive X-ray Spectroscopy (EDS) analysis of IZP-1.0.

For the Pd-containing samples, both IZP-0.50 and IZP-1.0 have rods smaller than half a micron and some axial layered agglomerate (Figure 22a and Figure 22b), similar to the morphology of the IZ-hydro (Figure 20). The elemental maps of In, Zr, and Pd in the IZP-1.0 sample show overlapping signals between the three elements indicating their homogeneous distributions in the sample (Figure 22c).

## 3.4 Surface area study

Table 5 Summary characterization table of all the synthesized catalysts: XRD, N<sub>2</sub> adsorption-desorption, CO<sub>2</sub>-TPD and O<sub>2</sub>-TPD. "n.d." stands for "non-detected".

		XRD	N₂ adsorptio	on-desorption	CO₂-TPD	02-	TPD
Name	Real Pd wt%	Crystallite size (nm)	S <sub>BET</sub> [m <sup>2</sup> /g]	Total pore V [cm³]	CO <sub>2</sub> adsorbed [μmol/g]	O <sub>2</sub> adsorbed [μmol/g]	CO <sub>2</sub> released during TPD [µmol/g]
I-comb	-	39	4.4	0.008	55	n.d.	<del>-</del>
I-hydro	-	12	47.4	0.095	149	27	-
I-ammo	-	13	54.8	0.128	274	34	-
IZ-comb	-	29	5.2	0.012	78	n.d.	-
IZ-hydro	-	16	58.4	0.145	242	27	-
IZ-ammo	-	12	69.6	0.184	399	28	-
IZ-carb	-	13	69.3	0.298	509	27	51
IZ-oxa	-	15	34.1	0.130	53	7	45
IZP-0.25	0.07	21	41.9	0.112	178	22	-
IZP-0.50	0.14	15	58.4	0.136	206	45	-
IZP-1.0	0.23	18	49.2	0.123	169	40	-
CZA-bench	-	-	39.3	0.136	-	-	-
Z-comb	-	-	3.0	0.009	-	-	-
Z-hydro	-	-	69.4	0.061	144	7	-
Z-ammo	-	-	54.3	0.123	279	8	-

## 3.4.1 N<sub>2</sub> adsorption-desorption analysis

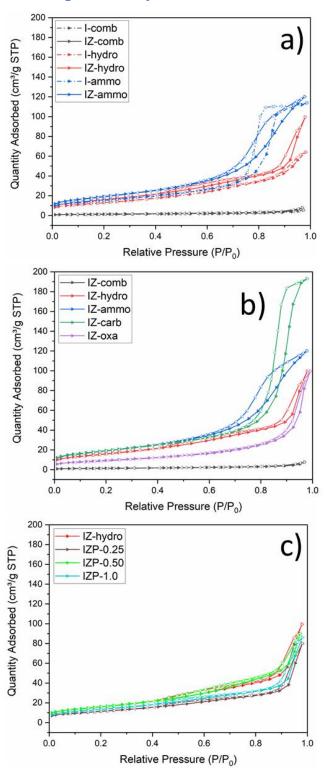


Figure 23 Isotherms of all the different catalysts synthesized: (a)  $In_2O_3$  and  $In_2O_3$ - $ZrO_2$  prepared by comb, hydro and ammo methods; (b) the whole  $In_2O_3$ - $ZrO_2$  catalysts series and (c)  $In_2O_3$ - $ZrO_2$ -Pd series prepared by hydro.

*Table 6*  $N_2$  *adsorption-desorption data.* 

	S <sub>BET</sub> [m <sup>2</sup> /g]	
I-comb	4.4	
I-hydro	47.4	
I-ammo	54.8	
IZ-comb	5.2	
IZ-hydro	58.4	
IZ-ammo	69.6	
IZ-carb	69.3	
IZ-oxa	34.1	
IZP-0.25	41.9	
IZP-0.50	58.4	
IZP-1.0	49.2	

Figure 23 presents the N<sub>2</sub>-physisorption isotherms of the different catalysts. The isotherms of the two combustion samples were attributed to type II, indicating a nonporous or macroporous solid. The isotherms of all the remaining catalysts were classified to type IV with H2 hysteresis loop according to IUPAC classification, which showed a characteristic of mesoporous materials. 104 The combustion method generated the materials having the specific surface area significantly lower than those prepared by the urea hydrolysis and the precipitation. The specific surface areas of I-comb and IZ-comb were 4.4 and 5.2 m<sup>2</sup> g<sup>-1</sup>, respectively (Table 6Table 5). These values were about 10-15-fold lower than those of other counterparts, e.g., 47.4 m<sup>2</sup> g<sup>-1</sup> of I-hydro and 69.6 m<sup>2</sup> g<sup>-1</sup> of IZ-ammo. Remarkably, the mixed oxides of In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> catalysts always had higher specific surface areas than their In<sub>2</sub>O<sub>3</sub> counterparts for all three synthesis methods. This implied that the inclusion of ZrO<sub>2</sub> improved the specific surface area of the catalysts. For the precipitation using different Na-containing precipitating agents, the IZcarb had a specific surface area almost the same as the IZ-ammo whereas the IZ-oxa had a surface area of only half of the IZ-carb. For the IZP series, the IZP-0.5 had the same surface area of 58.4 m<sup>2</sup> g<sup>-1</sup> as the IZ-hydro (the one without Pd) whereas IZP-0.25 and IZP-1.0 had surface areas of 41.9 and 49.2 m<sup>2</sup> g<sup>-1</sup>, respectively.

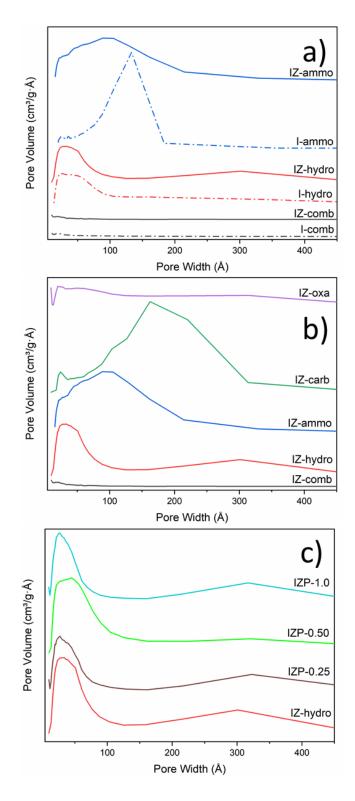


Figure 24 Pore Size Distribution (PSD) of all the different catalysts synthesized: (a)  $In_2O_3$  and  $In_2O_3$ - $ZrO_2$  prepared by comb, hydro and ammo methods; (b) the whole  $In_2O_3$ - $ZrO_2$  catalysts series and (c)  $In_2O_3$ - $ZrO_2$ -Pd series prepared by hydro.

The adsorption branch of the isotherms was used to calculate the pore distribution using the BJH method and the results are shown in Figure 24: both two samples prepared by the combustion method (I-comb and IZ-comb) showed a negligible pore volume; I-ammo and I-

hydro showed an average pore size of 5 and 14 nm, respectively; IZ-hydro had not only the main pore distribution around 14 nm as the I-hydro but also a broad peak around 30 nm; IZ-ammo showed a broader peak than that of the I-ammo but a smaller average pore size of I-ammo (10 nm versus 14 nm). These results indicate that the presence of Zr modified the porosity of the mixed oxides compared to pure In<sub>2</sub>O<sub>3</sub> oxides (Figure 24a).

Both IZ-carb and IZ-oxa had a wide range of pore distribution. However, the former showed two typical peaks at 4 and 19 nm whereas the latter showed no clear peak (Figure 24b). For the IZP series, three Pd-containing samples showed a narrow intensive peak around 14 nm and one broad weak at 30 nm (Figure 24c).

#### **3.4.2** CO<sub>2</sub>-TPD (Temperature Programmed Desorption)

Table 7 CO<sub>2</sub> released by different catalysts during CO<sub>2</sub>-TPD, previously adsorbed in the analysis.

	CO <sub>2</sub> adsorbed [μmol/g <sub>cat</sub> ]
I-comb	55
I-hydro	149
I-ammo	274
IZ-comb	78
IZ-hydro	242
IZ-ammo	399
IZ-carb	509
IZ-oxa	53
IZP-0.25	178
IZP-0.50	206
IZP-1.0	169

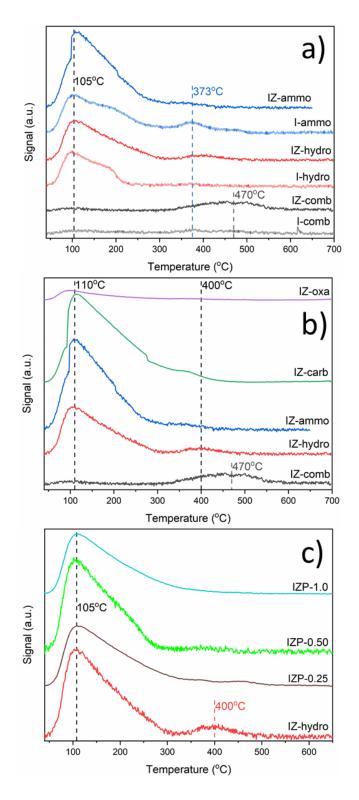


Figure 25  $CO_2$  Temperature Programmed Desorption ( $CO_2$ -TPD) graphs that depict the  $CO_2$  desorbed, during a temperature ramp, by: (a)  $In_2O_3$  and  $In_2O_3$ -Zr $O_2$  prepared by comb, hydro, and ammo methods; (b) the whole  $In_2O_3$ -Zr $O_2$  catalysts series and (c)  $In_2O_3$ -Zr $O_2$ -Pd series prepared by hydro.

Figure 25 presents the CO<sub>2</sub>-TPD profiles of different catalysts. For In<sub>2</sub>O<sub>3</sub>, the profile of the I-comb was almost flat while the profiles of I-ammo and I-hydro showed one broad and overlapped peak centered at around 105 °C and one weak peak around 373 °C. The CO<sub>2</sub> uptake

of I-ammo and I-hydro was 5-fold and 3-fold higher than that of the I-comb (Table 7). The IZ-comb, IZ-hydro, and IZ-ammo had a similar CO<sub>2</sub>-TPD profile to the profiles of their In<sub>2</sub>O<sub>3</sub> counterparts, being, however, more intense (Figure 25a). As a result, the CO<sub>2</sub> uptakes of the IZ samples were about 41 - 62 % higher than those of the pure In<sub>2</sub>O<sub>3</sub> counterparts (Table 7). The IZ-oxa showed a very weak profile of CO<sub>2</sub>-TPD while the IZ-carb had the broadest peak (up to 450 °C, Figure 25b). As a result, the IZ-carb had the highest uptake of CO<sub>2</sub> (509 μmol g<sup>-1</sup>) which was almost 10-fold higher than that of the IZ-oxa. For the IZP series, the profiles of the Pd-containing samples showed only one broad peak at around 105 °C with an absence of a second peak at high temperature as observed in the profile of IZ-hydro, without Pd (Figure 25c). The CO<sub>2</sub> uptakes of the IZP samples were in a range of 169 – 178 μmol g<sup>-1</sup>) and without a clear trend in correlation with Pd loading (Table 7).

#### **3.4.3** O<sub>2</sub>-TPD (Temperature Programmed Desorption)

Table 8  $O_2$  released by different catalysts during  $O_2$ -TPD, previously adsorbed in the analysis. "n.d." stands for "non-detected".

	O <sub>2</sub> adsorbed [μmol/g <sub>cat</sub> ]
I-comb	n.d.
I-hydro	27
I-ammo	34
IZ-comb	n.d.
IZ-hydro	27
IZ-ammo	28
IZ-carb	27
IZ-oxa	7
IZP-0.25	22
IZP-0.50	45
IZP-1.0	40

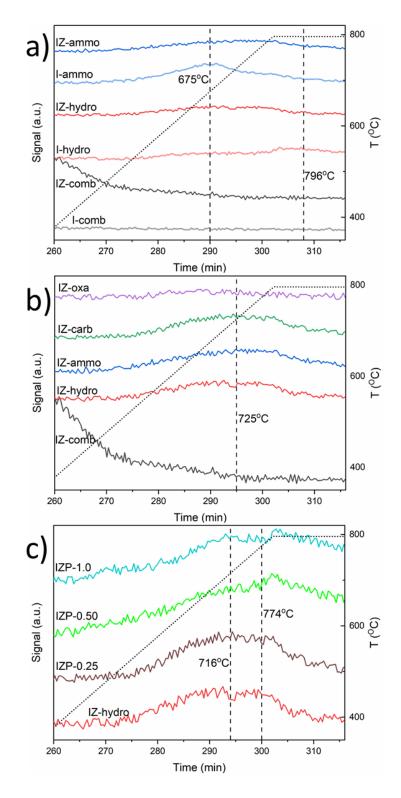


Figure 26  $O_2$  Temperature Programmed Desorption ( $O_2$ -TPD) graphs that depict the  $O_2$  desorbed, during a temperature ramp, by: (a)  $In_2O_3$  and  $In_2O_3$ - $ZrO_2$  prepared by comb, hydro, and ammo methods; (b) the whole  $In_2O_3$ - $ZrO_2$  catalysts series and (c)  $In_2O_3$ - $ZrO_2$ -Pd series prepared by hydro.

Figure 26 presents the  $O_2$ -TPD profiles of different catalysts. All the profiles showed  $O_2$  desorption peaks above 670 °C which is far from the temperature range between 250 and 350 °C for the catalytic test. The  $O_2$  desorbed values were around 30  $\mu$ mol/g, except for I-comb,

IZ-comb, and IZ-oxa whose had negligible uptakes of  $O_2$ . The IZP-0.5 and IZP-1.0 had higher uptake of  $O_2$ , perhaps due to the release of  $O_2$  from PdO.<sup>105</sup>

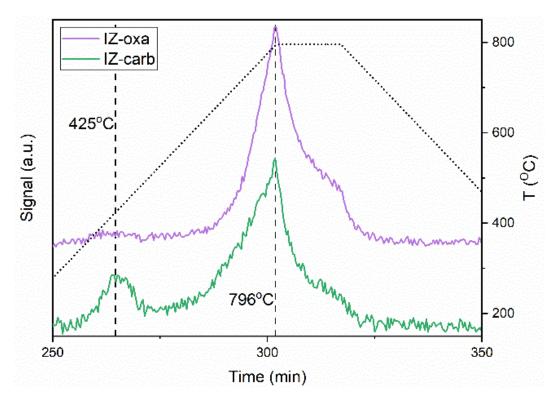


Figure 27 CO<sub>2</sub> released by IZ-carb and IZ-oxa during the O<sub>2</sub>-TPD, caused by residues of the C-containing precipitating agents used during their synthesis.

The mass number of  $CO_2$  (m/z = 44) was also tracked to investigate whether  $CO_2$  could be released during the  $O_2$ -TPD measurements for IZ-carb and IZ-oxa since C-containing precipitating agents (sodium carbonate and sodium oxalate) were used during the catalyst preparation. The IZ-oxa showed two distinct peaks of  $CO_2$  desorption at 425 and 780 °C whereas the IZ-carb released  $CO_2$  with one peak at around 780 °C (Figure 27). It was noted that these catalysts were calcined at 500 °C for 6 h. The data suggested that a part of carbon sources was still stable in the structure of the catalyst above the calcination temperature at 500 °C and this was desorbed at 780 °C as observed in the  $O_2$ -TPD. Moreover, after calcination, the IZ-oxa might adsorb again  $CO_2$  from the atmosphere and this perhaps explained the desorption of  $CO_2$  at 425 °C observed in the  $O_2$ -TPD profile.

## 3.5 Redox properties study

## 3.5.1 H<sub>2</sub>-TPR (Temperature Programmed Reduction)

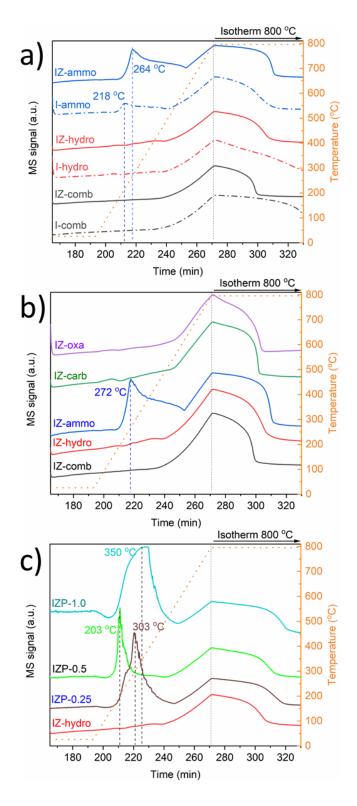


Figure 28 Temperature Programmed Reduction ( $H_2$ -TPR) of (a)  $In_2O_3$  and  $In_2O_3$ -Zr $O_2$  prepared by comb, hydro and ammo methods; (b) the whole  $In_2O_3$ -Zr $O_2$  catalysts series and (c)  $In_2O_3$ -Zr $O_2$ -Pd series prepared by hydro.

H<sub>2</sub>-TPR is a useful technique to study the redox properties of a solid sample: Figure 28 presents the H<sub>2</sub>-TPR profiles of different catalysts. Pure ZrO<sub>2</sub> showed a negligible consumption of H<sub>2</sub> with a flat profile during the analysis. The profile of I-comb and I-hydro showed only one reduction feature at a high-temperature range of 400 – 800 °C whereas the profile of I-ammo had also another peak at around 270 – 295 °C (Figure 28a). The peak at low temperature is associated with the reduction of surface In<sub>2</sub>O<sub>3</sub> while the peak at high temperatures could be attributed to the reduction of bulk In<sub>2</sub>O<sub>3</sub>. 45,102 The profiles of IZ samples showed similar features as their pure In<sub>2</sub>O<sub>3</sub> counterparts. The synthesis method using ammonia solution as precipitating agent facilitates a reduction of In<sub>2</sub>O<sub>3</sub> at lower temperatures, on the contrary of all the other preparation methods (Figure 28b). For the IZP series, all three Pd-containing samples showed two temperature peaks in the profile, unlike the one without Pd (IZ-hydro) which had only one reduction peak at high temperature (Figure 28c). This could be attributed to the reduction of either PdO or the surface In<sub>2</sub>O<sub>3</sub>. However, PdO was usually reduced at temperatures lower than 200 °C<sup>65,66,106</sup> and the loadings of Pd were substantially low. Therefore, the low-temperature peaks in these catalysts were likely involved in the reduction of surface In<sub>2</sub>O<sub>3</sub>, indicating that Pd can induce such a reduction.

### 3.5.2 X-ray Photoelectron Spectroscopy (XPS) analysis

Table 9 Ratio (%) of different oxygen (O) species deconvoluted from O1s binding energy

	Lattice O (%)	O-defect (%)	Surface O (%)
I-comb	72	17	12
I-hydro	68	21	11
I-ammo	71	18	12
IZ-comb	62	29	9
IZ-hydro	67	24	9
IZ-ammo	86	7	7
IZ-oxa	78	18	7
IZ-carb	77	19	5
IZP-1.0	71	21	9

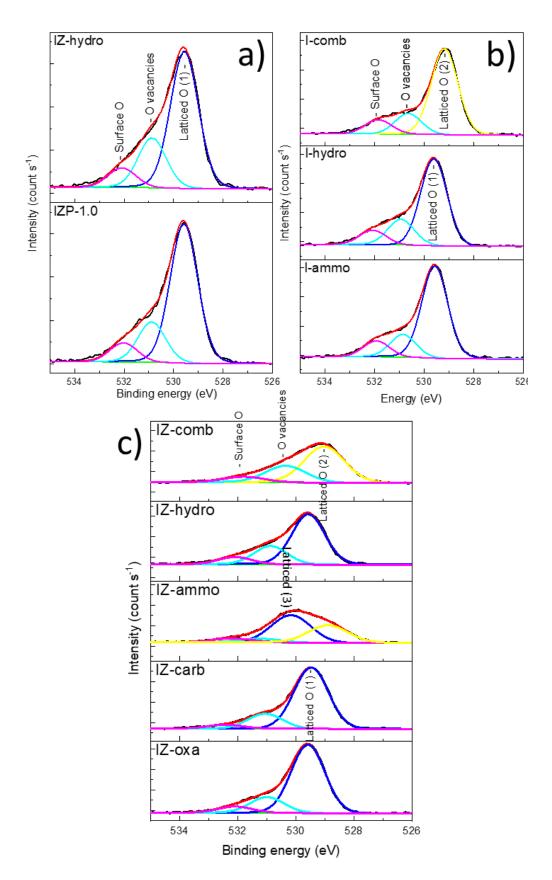


Figure 29 X-ray Photoelectron Spectroscopy (XPS) O1s of (a)  $In_2O_3$ - $ZrO_2$  and  $In_2O_3$ - $ZrO_2$ -Pd prepared by hydro (IZ-hydro and IZP-1.0); (b) the whole  $In_2O_3$  catalysts series and (c) the whole  $In_2O_3$ - $ZrO_2$  series.

X-ray Photoelectron Spectroscopy (XPS) was performed to investigate the redox surface properties of the catalysts. The O1s core level spectra of the catalysts are shown in Figure 29. The peak of O1s of each sample can be deconvoluted into three peaks around 529 - 530 eV, 530.5 - 531.5 eV, and 532 - 533 eV corresponding to O-lattice, O-defect (O<sub>v</sub>), and O-adsorbed species, respectively. All the samples showed a similar distribution of oxygen species (Table 9): 62 - 77 % for lattice O, 5 - 12 % of surface O, and 18 - 29 % of O<sub>v</sub>. The only exception appears to be IZ-ammo, with an 86 % of O-lattice (considering both In<sub>2</sub>O<sub>3</sub> and ZrO<sub>2</sub>), 7 % of O-defect, and another 7 % as O<sub>v</sub>.

The In3d<sub>5/2</sub> showed the binding energy around 444 eV which attributed to the oxidation state of +3 of In in all the samples. The XPS-Pd of IZP-1.0 had too much background noise and the Pd signal was too weak to be detected, most certainly for the low wt.% loading of Pd in the catalyst.

## 3.6 Catalytic test

The catalytic activity of different catalysts for CO<sub>2</sub> hydrogenation was performed in a fixed-bed reactor operated in a temperature range from 250 to 350 °C and pressure of 40 bars. The mass of each catalyst was normalized to obtain the same amount of 500 mg of Indium for comparison purposes. During the tests, CH<sub>3</sub>OH was produced via CO<sub>2</sub> hydrogenation (Reaction (7)) and CO was generated via reverse water-gas shift reaction (RWGS, Reaction (8)):

(7) 
$$CO_2 + 3H_2 \rightleftharpoons CH_3OH + H_2O$$
,  $\Delta H^{\circ} = -49.4 \text{ kJ mol}^{-1}$ 

(8) 
$$CO_2 + H_2 \rightleftharpoons CO + H_2O$$
,  $\Delta H^{\circ} = -41.2 \text{ kJ mol}^{-1}$ 

The reaction (7) generally follows the formate (HCOO\*) pathway<sup>49,56</sup> and thus CH<sub>4</sub> is likely formed as a by-product (Reaction (9)), since hydrogenation of CO<sub>2</sub> to methane is possibly involved in a similar pathway:<sup>108</sup>

(9) 
$$CO_2 + 4H_2 \rightleftharpoons CH_4 + 2H_2O$$
,  $\Delta H^{\circ} = -165.0 \text{ kJ mol}^{-1}$ 

In all the catalytic tests in this study, CH<sub>3</sub>OH and CO were the main products whereas CH<sub>4</sub> was only found in some cases. However, the maximum selectivity of CH<sub>4</sub> was lower than 2.5% in all tests, and hence the selectivity in CH<sub>4</sub> was not reported in the results to simplify the evaluation. The comparison of the catalytic activity between the catalysts was assessed in terms

of  $CO_2$  conversion ( $X_{CO_2}$ ),  $CH_3OH$  selectivity ( $S_{CH_3OH}$ ), and space-time yield of  $CH_3OH$  ( $STY_{CH_3OH}$ ). For comparison purposes, the catalytic test of the benchmark CZA-bench catalyst was also performed.

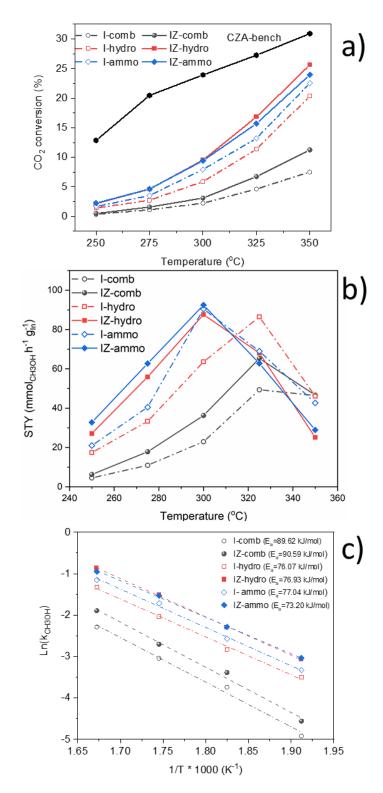


Figure 30 Comparison of  $In_2O_3$  and  $In_2O_3$ - $ZrO_2$  catalysts on (a)  $CO_2$  conversion, (b) STY of  $CH_3OH$ , and (c) apparent activation energy.

Figure 30 presents the activity performance of  $In_2O_3$  and  $In_2O_3$ - $ZrO_2$  prepared by combustion, urea hydrolysis, and precipitation with NH<sub>4</sub>OH solution. For all catalysts, CO<sub>2</sub> conversion increased substantially as increasing temperature from 250 to 350 °C (Figure 30a). For sole  $In_2O_3$ , the CO<sub>2</sub> conversion increased with an order of I-comb << I-hydro < I-ammo in the whole range of temperature from 250 to 350 °C (Figure 30a, dashed lines).

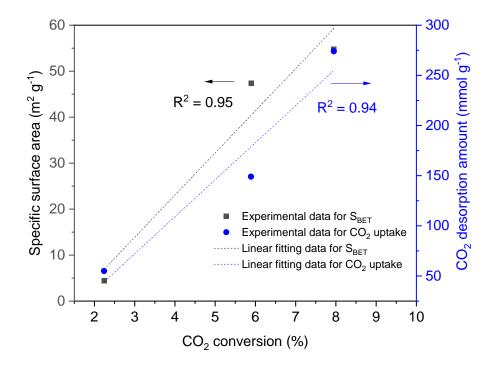


Figure 31 Fitting of  $CO_2$  conversion with both the specific surface areas and  $CO_2$  desorption amount during  $CO_2$ -TPD.

The CO<sub>2</sub> conversions were linearly fit with both the specific surface areas and CO<sub>2</sub> desorption amount (Figure 31), suggesting the specific surface area plays a crucial role in the CO<sub>2</sub> conversion since all three catalysts had the same cubic structure of In<sub>2</sub>O<sub>3</sub> (Figure 18). Significantly low conversion of CO<sub>2</sub> on I-comb catalyst was accounted by a substantially low specific surface area of the catalyst. It is noted that the CO<sub>2</sub> conversions of I-hydro and I-ammo are better to some extent than those reported in the literature under similar or milder reaction conditions (Table 10). For example, In<sub>2</sub>O<sub>3</sub> prepared by the precipitation with Na<sub>2</sub>CO<sub>3</sub> showed a conversion of 11.8% at 350 °C under similar reaction conditions, <sup>109</sup> whereas other works reported much lower CO<sub>2</sub> conversion even under milder reaction conditions (e.g., lower WHSH, reactants diluted with inert gasses, ...). <sup>102,110</sup> Both I-hydro and I-ammo catalysts showed CH<sub>3</sub>OH selectivity of 42-45% for temperature 250-300 °C and the selectivity decreased rapidly with a further increase in temperatures due to thermodynamic favor for RWGS reaction. The I-comb catalyst also had a similar value of CH<sub>3</sub>OH selectivity as I-hydro and I-ammo at temperatures from 250-350 °C but it lost CH<sub>3</sub>OH selectivity when the

temperature was higher than 325 °C. The yield of CH<sub>3</sub>OH production on each catalyst is a trade-off between the CO<sub>2</sub> conversion and CH<sub>3</sub>OH selectivity due to a competition between the methanol generation reaction and the RWGS reaction. As a result, the maximum CH<sub>3</sub>OH production rate calculated per gram of Indium (mmol<sub>CH3OH</sub> g<sub>In</sub><sup>-1</sup> h<sup>-1</sup>) was ranked in increasing order of I-comb (49.37 at 325 °C) < I-hydro (86.44 at 325 °C) < I-ammo (90.42 at 300 °C). The CH<sub>3</sub>OH production rates normalized with the mass of the catalysts were 40.80, 71.43, and 74.73 mmol<sub>CH3OH</sub> g<sub>cat</sub><sup>-1</sup> h<sup>-1</sup> for I-comb, I-hydro, and I-ammo, respectively. This implies that the preparation method strongly influences the catalytic performance for CO<sub>2</sub> hydrogenation to CH<sub>3</sub>OH. It is noted that the CH<sub>3</sub>OH production rates for I-hydro and I-ammo are promising compared to those reported for In<sub>2</sub>O<sub>3</sub> catalysts in the literature (Table 10). In the literature, CO<sub>2</sub> conversion, methanol selectivity, and methanol formation are usually correlated to the content of O vacancy;<sup>35,44,52</sup> however, in this work the correlation between O vacancy and the methanol production rate was not clear.

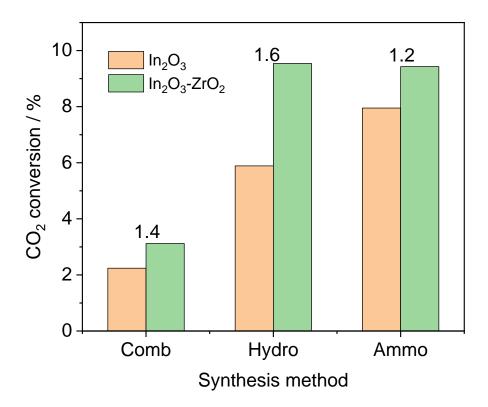


Figure 32 Comparison of In<sub>2</sub>O<sub>3</sub>'s and In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub>'s CO<sub>2</sub> conversion of catalysts synthesized with the same preparation method.

The apparent activation energies calculated from Arrhenius plots (for the conversion of CO<sub>2</sub> below 20%) were approximately 90, 76, and 77 kJ mol<sup>-1</sup> for I-comb, I-hydro, and I-ammo, respectively (Figure 30c). Different values of activation energy for CO<sub>2</sub> hydrogenation on cubic In<sub>2</sub>O<sub>3</sub> catalysts have been reported in the literature, <sup>110</sup> e.g., from 55 to 101 kJ mol<sup>-1</sup>. It should

be noted that it is only fair when comparing the apparent activation energy for catalysts tested under similar reaction conditions because the apparent activation energy values depend on not only the type of catalysts but also the operating conditions, i.e., feed compositions and treatment conditions. Similar values of activation energy for I-hydro and I-ammo suggest that the reaction mechanism was perhaps similar for both catalysts.

Each mixed oxide of In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> catalyst prepared by three different methods showed higher CO<sub>2</sub> conversion than that on its In<sub>2</sub>O<sub>3</sub> counterpart (Figure 32; Figure 30a, each lines pair with the same color). This indicated the advantage of ZrO<sub>2</sub> support in the mixed oxide In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> catalysts. IZ-hydro and IZ-ammo catalysts showed very similar CO<sub>2</sub> conversion up to 300 °C but IZ-hydro gets over IZ-ammo at higher temperatures (Figure 30a, solid lines). Both catalysts outperformed the IZ-comb for the conversion of CO<sub>2</sub> from 250 to 35 °C. This indicates that the preparation method significantly influences the CO<sub>2</sub> conversion for In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> catalysts likely for the In<sub>2</sub>O<sub>3</sub> series. Both IZ-hydro and IZ-ammo showed the maximum rate of CH<sub>3</sub>OH at 300 °C, 87.61 and 92.44 mmol g<sub>In</sub><sup>-1</sup> h<sup>-1</sup>, respectively, whereas IZ-comb had the maximum rate of CH<sub>3</sub>OH about 65.30 mmol g<sub>In</sub><sup>-1</sup> h<sup>-1</sup> at 325 °C. It is noted that the IZ-hydro had a mixed phase of rhombohedral and cubic In<sub>2</sub>O<sub>3</sub> while IZ-ammo possessed only cubic In<sub>2</sub>O<sub>3</sub>; however, they had similar CO<sub>2</sub> conversion and CH<sub>3</sub>OH yield, suggesting that there seemed to have no significant difference in the activity between the two phases. In the literature, cubic In<sub>2</sub>O<sub>3</sub> has been reported to be more active than rhombohedral In<sub>2</sub>O<sub>3</sub> without support. <sup>110</sup> The discrepancy may be related to the role of ZrO2 in our catalysts. A high CH3OH formation rate for In2O3-ZrO<sub>2</sub> than the In<sub>2</sub>O<sub>3</sub> counterpart was correlated to the enhancement of ZrO<sub>2</sub> to the specific surface area and CO<sub>2</sub> adsorbed amount. Furthermore, the apparent activation energy of In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> was close to that of In<sub>2</sub>O<sub>3</sub> counterpart prepared with the same synthesis method, indicating a similar reaction pathway between each pair of the catalysts.

The catalytic performance of a benchmark CuZnAl catalyst (Cu/Zn/Al = 60/30/10 molar ratio) was also performed and compared with In<sub>2</sub>O<sub>3</sub> and In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> catalysts. The CuZnAl catalyst had a much higher CO<sub>2</sub> conversion than the Indium-based catalyst. However, this catalyst favored strongly the RWGS, especially at a temperature higher than 300 °C and as a result, it showed a lower CH<sub>3</sub>OH yield than IZ-hydro, IZ-ammo, and I-ammo from 300 to 350 °C (Figure 30b). This is the advantage of an Indium-based catalyst compared to a Cu-based catalyst for CO<sub>2</sub> hydrogenation to CH<sub>3</sub>OH.<sup>112</sup>

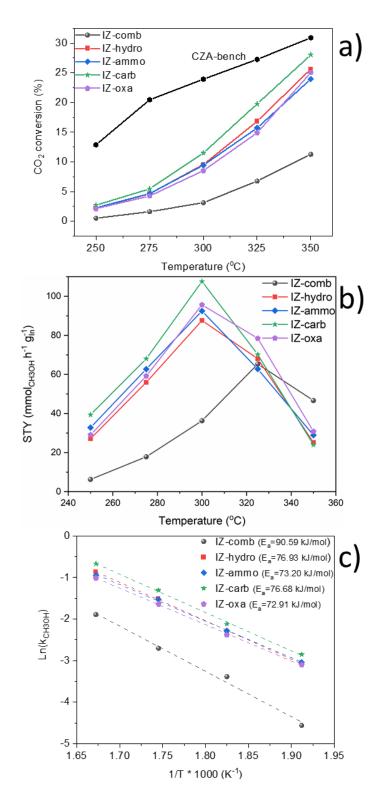


Figure 33 Comparison of In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> catalysts on (a) CO<sub>2</sub> conversion, (b) STY of CH<sub>3</sub>OH, and (c) apparent activation energy.

Three synthesis methods, namely combustion, urea hydrolysis, and precipitation with NH<sub>4</sub>OH, are free-sodium routes. To extend further the effect of the synthesis method, other two catalysts of In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> were synthesized with precipitation using Na<sub>2</sub>CO<sub>3</sub> and Na<sub>2</sub>C<sub>2</sub>O<sub>4</sub> as precipitating agents and tested for CO<sub>2</sub> hydrogenation to CH<sub>3</sub>OH. A comparison of the catalytic performance

of these two catalysts IZ-carb and IZ-oxa with others is shown in Figure 33. IZ-oxa showed comparable performance with IZ-hydro and IZ-ammo in terms of CO<sub>2</sub> conversion (Figure 33a), CH<sub>3</sub>OH yield, and formation rate whereas the IZ-carb was the best among five samples of In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub>. This catalyst had an 11.49 % conversion of CO<sub>2</sub>, 4.22 % yield of CH<sub>3</sub>OH at 300 °C, and a methanol STY of 107.54 mmol g<sub>In</sub>-1 h<sup>-1</sup>. The best activity of IZ-carb may be related to the textural properties, for example, large specific surface and substantially large in total pore volume compared to those of the others (Table 5). However, the textural properties may not account entirely for a comparable rate of CH<sub>3</sub>OH formation with the IZ-hydro and IZ-ammo since the IZ-oxa had a specific surface area of approximately half of IZ-hydro and IZ-ammo.

In this study, three catalysts of In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> with different Pd loadings were prepared with the urea hydrolysis method and the results of the catalytic activity are shown in Figure 34. Note that the real loading of Pd in each sample was lower than the nominal one with a factor of 4.8 (Table 3). Both IZP-0.25 and IZP-0.5 had a higher conversion and CH<sub>3</sub>OH selectivity than the sample without Pd (IZ-hydro) whereas the IZP-1.0 had lower CH<sub>3</sub>OH selectivity at temperatures higher than 275 °C. Overall, the maximum rate of CH<sub>3</sub>OH formation was ranked in increasing order of IZ-hydro < IZP-1.0 < IZP-0.25 < IZP-0.5. All catalysts had comparable apparent activation energy in a range of 73-77 kJ mol<sup>-1</sup> indicating a similar reaction mechanism (Figure 34c). The catalytic performance suggests that the incorporation of Pd enhanced the CH<sub>3</sub>OH selectivity but with a certain loading, e.g., 0.14 wt.%, whereas a high loading (e.g., 0.25 wt.%) favored more CO selectivity and thus decreased the space-time yield of CH<sub>3</sub>OH. We hypothesized that the best performance of IZP-0.5 is perhaps related to three main factors including high specific surface area, ease of reduction, and its optimum cluster size of Pd compared to IZP-1.0. It has been reported in the literature that the size of the Pd cluster is very important to restrict the RWGS reaction on Pd sites and the Pd cluster size strongly depends on the preparation method.<sup>66</sup> The CH<sub>3</sub>OH formation rate of IZP-0.5 was very promising compared to those reported in the literature for Pd-containing catalysts (Table 10).

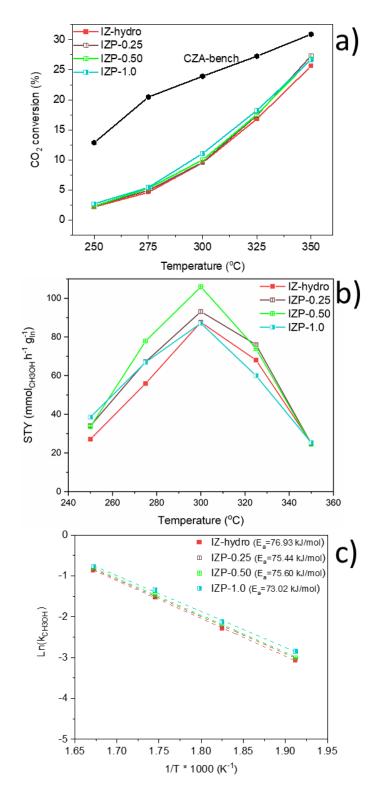


Figure 34 Comparison of In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub>-Pd catalysts on (a) CO<sub>2</sub> conversion, (b) STY of CH<sub>3</sub>OH, and (c) apparent activation energy.

### 3.6.1 Activity comparison with literature

In Table 10 below, there is a summary table that compares the activity performances of the catalysts studied in this project (bottom of the table) and the catalysts studied in the recent literature (top of the table):

Table 10 Comparison of the activity performance of the catalysts reported in this study and recent literature (\*per grams of In).

Catalysts	CO <sub>2</sub> /H <sub>2</sub> /inert (v/v)	Space velocity		Pressure	Temperature	CO <sub>2</sub> conversion	CH <sub>3</sub> OH formation		
		GHSV	WHSV	(MPa)	(K)	(%)	STY	Selectivity	Ref
	(V/V)	(h <sup>-1</sup> )	(L g <sup>-1</sup> h <sup>-1</sup> )	(MIF a)	( <b>K</b> )	(70)	(mmol gcat <sup>-1</sup> h <sup>-1</sup> )	(%)	
In <sub>2</sub> O <sub>3</sub>	1/4	16000	26	5	573	-	ca. 6.3	100	42
In <sub>2</sub> O <sub>3</sub> /ZrO <sub>2</sub>	1/4	16000	26	5	573	5.2	9.2	100	
In <sub>2.5</sub> /ZrO <sub>2</sub>	1/4/1.67	24000		5	523	0.9	1.1	74	55
Hexagonal-In <sub>2</sub> O <sub>3</sub>	1/3/0.55	-	21.6	4	598	4.4	6.3	68	113
Pd/In <sub>2</sub> O <sub>3</sub> (precipitate)	1/4/0	-	21	5	573	20	27.8	70	45
Pd/In <sub>2</sub> O <sub>3</sub> (Impregnation)	1/4/0	-	21	5	573	18	25.0	70	
In:Pd (2:1)/SiO <sub>2</sub>	1/4/1.5	-	7.5	4	573	-	18.4	61	65
Pd- In <sub>2</sub> O <sub>3</sub> (CP)	1/4/0	-	48	4	553	-	31.6	78	66
1.5Y9In/ZrO <sub>2</sub>	1:4/1.5	-	52	4	573	7.6	13.1	69	107
3La10In/ZrO2	1/4/1.5	-	52	4	573	7.7	13.1	66	
In <sub>2</sub> O <sub>3</sub>	1/3/1	-	9	2	593	~5	14.6	~39	102
20In/ZrO <sub>2</sub> -800	1/3/1	-	9	2	593	~5	59.6	~51	
c-In <sub>2</sub> O <sub>3</sub>	1/4/0	-	16	4	613	~ 12	3.0	20	110
rh-In <sub>2</sub> O <sub>3</sub>	1/4/0	-	16	4	613	~ 5	1.8	30	
In <sub>2</sub> O <sub>3</sub> -commercial	1/3/1	-	15	4	543	1.1	0.8	55	43
In <sub>2</sub> O <sub>3</sub> -commercial	1/3/1	-	15	4	603	7.1	3.7	40	
In <sub>2</sub> O <sub>3</sub> (hydrolysis)	1/3/0	-	12*	4	598	11.4	2.8*	31	
In <sub>2</sub> O <sub>3</sub> (carbonate)	1/3/0	-	12*	4	573	9.5	2.8*	36	This work
In <sub>2</sub> O <sub>3</sub> -ZrO <sub>2</sub> -hydro	1/3/0	-	12*	4	573	11.5	3.5*	37	THIS WOLK
Pd- In <sub>2</sub> O <sub>3</sub> -ZrO <sub>2</sub> -hydro	1/3/0	-	12*	4	573	10.0	3.4*	42	

#### 3.6.2 Stability test

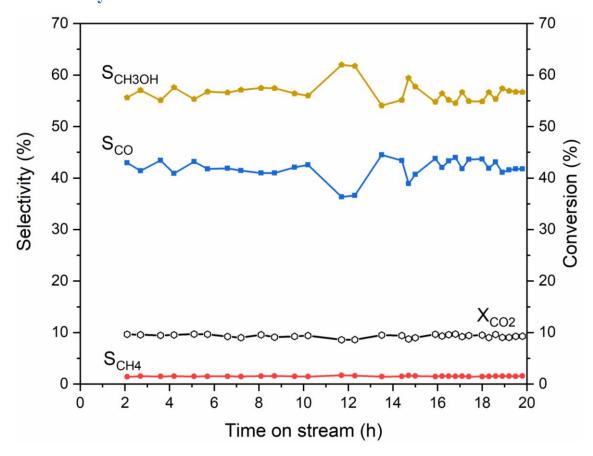


Figure 35 IZP-0.50 stability test over 20 hours.

A stability test was performed on the catalyst IZP-0.50 at 300 °C for 20 h and the data are presented in Figure 35. At the beginning of the test, the conversion of  $CO_2$  ( $X_{CO2}$ ) was approximately 9.6 % and the selectivity in  $CH_3OH$  ( $S_{CH3OH}$ ) and CO ( $S_{CO}$ ) was 42.3 % and 56.2 %, respectively. The selectivity in  $CH_4$  ( $S_{CH4}$ ) was negligible (less than 1.5 %). Almost the same values of  $CO_2$  conversion and the selectivity were observed after 20 h of time-onstream, suggesting that the catalyst was stable during the test:  $X_{CO2}$  was 9.3 %,  $S_{CH3OH}$ ,  $S_{CO}$ , and  $S_{CH4}$  were 41.8 %, 56.7 %, and 1.6 %, respectively. The selectivity in  $CH_4$  was negligible (less than 1.5 %). Under this condition, the space-time yield of  $CH_3OH$  of the IZP-0.5 catalyst was 1.89  $g_{MeOH}$  h<sup>-1</sup>  $g^{-1}_{catalyst}$  (3.32  $g_{MeOH}$  h<sup>-1</sup>  $g^{-1}_{Indium}$ ), higher than the successful stability test result with a Pd-promoted  $In_2O_3$  catalyst, reported by Frei, *et al.*<sup>66</sup> in 2019 (0.96  $g_{MeOH}$  h<sup>-1</sup>  $g^{-1}_{catalyst}$ ), that employed different operating conditions.

#### 3.7 Post-reaction characterization

Some of the used catalysts were selected and analyzed with XRD, N<sub>2</sub> physisorption, and XPS to investigate any changes in the structure and surface composition of the catalysts after the reactions. The properties of the different spent catalysts are listed in Table 11 hereafter:

	Fresh catalyst	Spent catalyst		
	XRD crystallites size (nm)	S <sub>BET</sub> [m²/g]	XRD crystallites size (nm)	S <sub>BET</sub> [m <sup>2</sup> /g]
I-hydro	12	47.4	14	25.2
I-ammo	13	54.8	17	32.2
IZ-hydro	16	58.4	21	35.5
IZ-ammo	12	69.6	14	58.6
IZ-carb	13	69.3	12	58.5
IZ-oxa	15	34.1	-	29.4
IZP-0.25	21	41.9	-	28.4
IZP-0.50	15	58.4	15	34.6
IZP-1.0	18	49.2	21	32.9

Table 11 Characterization table of different spent catalysts

## 3.7.1 X-Ray Diffraction (XRD)

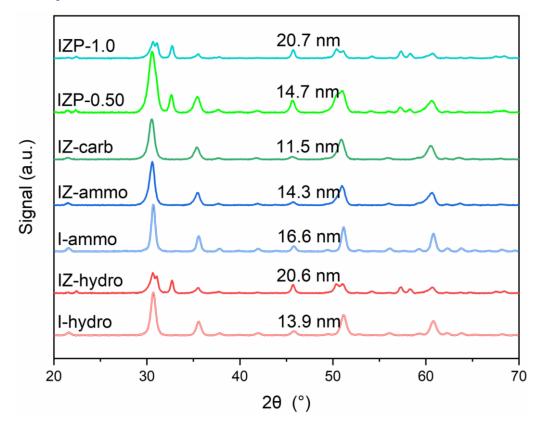


Figure 36 X-Ray Diffraction (XRD) of different spent catalysts. The crystallites sizes, calculated for the plane (431), are marked in the graph.

Figure 36 presents the XRD patterns of the spent catalysts. The used catalyst showed the same XRD pattern as its fresh counterpart, suggesting there was no change in the structure of the catalyst after the reaction. However, the crystalline size calculated from the Scherrer equation for the plane (431) was slightly increased from 1-5 nm due to the sintering phenomenon, except for IZ-carb and IZP-0.50 (Table 11).

### 3.7.2 N<sub>2</sub> adsorption-desorption analysis

The porosity of the mesoporous material has not been modified with the catalytic test. Nevertheless, the specific surface areas were decreased by almost a half for all the catalysts and the total pore size volume drastically decreased for most of the catalysts studied, except for IZ-oxa, which did not show any change (Table 11).

## 3.7.3 X-ray Photoelectron Spectroscopy (XPS) analysis

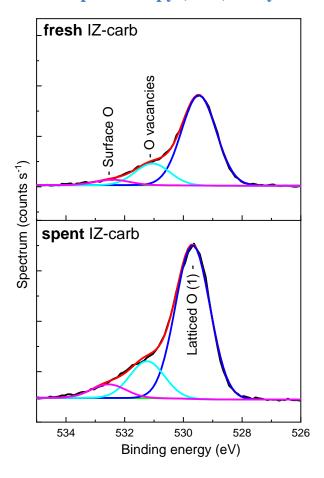


Figure 37 XPS of fresh and spent IZ-carb.

Table 12 XPS areas signal ratio for fresh and spent IZ-carb

Peak notation	Chemical states	IZ-carb-Fresh	IZ-carb-spent	
O1s	In <sub>2</sub> O <sub>3</sub>	77 %	75 %	
	Oxy. Vac. in $ZrO_2$ - rich/-like structure	18 %	18 %	
	Zr-OH	5 %	7 %	

XPS was carried out with the sample IZ-carb, both fresh and spent, after the catalytic test: its data suggested that the oxidation state of In remained identical, but since this XPS has been operated *ex-situ*, a re-oxidation by atmospheric conditions should not be excluded. The percentage of oxygen vacancy, as well, was not changed substantially (Figure 37 and Table 12); a similar trend in the O1s spectra has been reported previously.<sup>114</sup>

## 4. Conclusions

All the preparation methods adopted in this thesis were reliable for the synthesis of In-based catalysts, with the only exception of the urea combustion method (comb). During the comb synthesis, an In mass loss occurred together with the formation of two different oxides phases instead of the most common solid solution of In<sub>2</sub>O<sub>3</sub> and ZrO<sub>2</sub>; additionally, the comb samples had poor catalytic performance and poor textural properties. The same structure of cubic In<sub>2</sub>O<sub>3</sub> was found on the pure oxide samples regardless of the preparation methods, whereas all the other methods gave origin to a solid solution of In<sub>2</sub>O<sub>3</sub> and ZrO<sub>2</sub> with a cubic structure. This is not true for the urea hydrolysis method (hydro), which showed the formation of a different rhombohedral phase of In<sub>2</sub>O<sub>3</sub>, alongside the cubic solution, and a different morphology, of rods around 500 nm and some axial-layered agglomerate. In the In<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> series, the lower yield of methanol of the hydro sample, compared with the ammonia solution (ammo) and carbonate solution (carb) precipitation, might be related to the formation of the rhombohedral In<sub>2</sub>O<sub>3</sub> phase.

Looking at parameters as surface area, porosity,  $CO_2$  adsorption capabilities, and activity (STY, and  $X_{CO2}$ ), the preparation methods are ranked in this order: comb < oxa (oxalate solution precipitation) < hydro < ammo < carb, with the only exception of  $STY_{IZ-oxa}$ , second only to  $STY_{IZ-carb}$ . This last catalyst showed 11.5 % conversion of  $CO_2$ , 4.2 % yield of  $CH_3OH$  at 300 °C, and a methanol STY of 108 mmol  $g_{In}^{-1}$  h<sup>-1</sup>. The precipitation by using a carbonate solution as precipitating agent generated superior textural properties and remarkable activity. Finally, only the synthesis method using ammonia solution precipitation interestingly facilitates an  $In_2O_3$  reduction at lower temperatures.

The loading of Pd was smaller than expected, for the urea hydro method, which turned out to be unsuitable: Pd most probably formed a stable and water-soluble complex of Pd and ammonia that hindered its precipitation. As expected, the introduction of  $ZrO_2$  as a support by coprecipitation method is more than beneficial for the bulk  $In_2O_3$ . In some cases,  $In_2O_3$ - $ZrO_2$  also lowered the temperature at which the maximum yield of methanol was achieved. On the other hand, the loading Pd in the mixed oxide  $In_2O_3$ - $ZrO_2$  just had a limited effect among the tested samples due to the substantially narrow range distribution of the Pd loadings. IZ-hydro has better textural properties (0 wt.% of Pd loading) than the  $In_2O_3$ - $ZrO_2$ -Pd samples, which showed this trend: IZP-1.0  $\approx IZP$ -0.25 < IZP-0.50 < IZ-hydro. Despite this, the STY of methanol improved with the Pd loading: IZ-hydro  $\approx IZP$ -1.0 < IZP-0.50 < IZP-0.50. IZP-0.50.

had very promising performances compared to literature and excellent stability in a 20h-TOS stability test. The best performance of IZP-0.50 is perhaps related to three main factors including high specific surface area, ease of reduction, and its optimum Pd cluster size compared to IZP-1.0. All three Pd-containing samples showed a reduction at lower temperatures, possibly attributed to the reduction of either PdO or the surface In<sub>2</sub>O<sub>3</sub>.

For the spent catalysts we observed an overall increase in the crystallite size, except for IZ-carb and IZP-0.50, while the surface area decreased by almost half of the original value.

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